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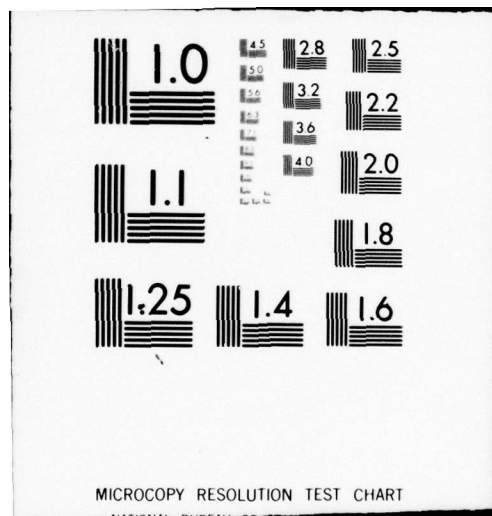
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Final Technical Report
May 1979

ELECTRONIC CHARACTERISTICS OF III-V COMPOUNDS

Massachusetts Institute of Technology

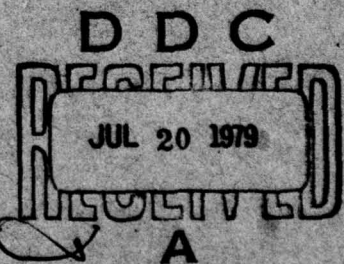
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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Our experimental and theoretical program has been aimed at the development of approaches and methods for the reliable electronic characterization of III-V compounds. We have investigated the determination of compositional, structural and electronic characteristics of GaAs and InP on a macro- and micro-scale. We have developed novel theoretical and experimental techniques for obtaining two-dimensional microprofiles of the carrier concentration in GaAs and InP (scanning IR absorption) and microprofiles of the minority carrier characteristics (SEM-EBIC mode). We have also developed convenient methods for the determination | | |

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of the compensation ratio and total concentration of ionized impurities which is based on electron mobility and free carrier absorption. Finally, we have initiated a comprehensive characterization study of InP in conjunction with crystal growth.

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Preface

Our experimental and theoretical program has been aimed at the development of approaches and methods for the reliable electronic characterization of III-V compounds. We have investigated the determination of compositional, structural and electronic characteristics of GaAs and InP on a macro- and micro-scale. We have developed novel theoretical and experimental techniques for obtaining two-dimensional microprofiles of the carrier concentration in GaAs and InP (scanning IR absorption) and microprofiles of the minority carrier characteristics (SEM-EBIC mode). We have also developed convenient methods for the determination of the compensation ratio and total concentration of ionized impurities which is based on electron mobility and free carrier absorption. Finally, we have initiated a comprehensive characterization study of InP in conjunction with crystal growth. Unfortunately, as a unique characterization framework was being brought to bear on the study of InP, the support of the work was unexpectedly terminated.

GENERAL REMARKS

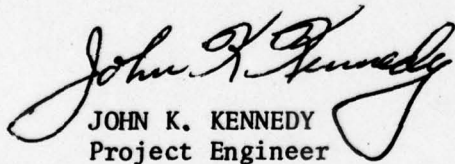
It is now generally accepted within the scientific and engineering community that to insure further progress in processing and application of semiconducting materials extensive work must be carried out on the characterization of the materials in direct correlation with crystal growth and device processing.

Accordingly, the first stage of our program was devoted to the development of theoretical and experimental characterization approaches and to the design and construction of experimental facilities which would fill the gap between the existing needs and the available methods for practical and highly reliable characterization of III-V compounds on a macro- and micro-scale. The characterization techniques and methods developed within the framework of the present grant are summarized in Table 1.

EVALUATION

This report is the final report on the contract. It covers research done on the Electronic properties of GaAs and InP during the period 1 Jan 77 to 30 Sep 78. The objective of the research was to investigate and determine on a macro- and micro-scale the compositional, structural, and electronic characteristics of GaAs and InP. Rigorous theoretical calculations of electron mobility and of free carrier absorption as a function of carrier concentration and the compensation ratio were carried out, verified experimentally and the results reduced to tabular form. A reliable determination of free carrier concentration and testing of sample homogeneity was developed using transport in high magnetic fields. Apparatus and theory were developed for profiling of carrier concentration and ionized impurities by scanning I.R. absorption. A method and apparatus were developed for profiling of diffusion length, lifetime and surface recombination velocity of the SEM-EBIC method.

The work is of value because it provides basic knowledge and techniques for the investigation of the electronic properties of GaAs and InP. An in-depth understanding of the electronic properties of these materials is essential for their use in optical and electronic communications and ECM systems.


JOHN K. KENNEDY
Project Engineer

DETERMINATION OF COMPENSATION RATIO AND
CONCENTRATION OF IONIZED IMPURITIES

The compensation ratio and impurity concentration are the parameters of key importance in semiconductor application and technology. Nevertheless, the existing methods for the determination of these parameters in III-V compounds have been either impractical or unreliable.

We have succeeded in the development of an accurate and convenient characterization approach based on low- and high-frequency transport phenomena in III-V compounds. Thus, we have carried out rigorous theoretical calculations of electron mobility and of free carrier absorption as a function of carrier concentration and the compensation ratio. These theoretical results have been verified experimentally and they have been utilized to establish the tables from which the compensation ratio can be directly obtained from carrier concentration and from mobility or infrared absorption coefficient. These tables, which are appended to this report, are far more accurate than those in use up to this time. A detailed account of the experimental and theoretical treatment for GaAs is given in the enclosed preprint on "Electron Mobility and Free Carrier Absorption in GaAs; Determination of the Compensation Ratio", (Journal of Applied Physics, in press). The results obtained with InP are being prepared for publication.

It has been recently reported that the compensating centers in GaAs are associated with point defects. Thus, our method for the determination of the compensation ratio can be used as a convenient means for the assessment of the quality of the material with respect to the overall density of point defects.

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TABLE 1. Techniques and Methods Developed for the Characterization of III-V Compounds

| METHOD | CHARACTERIZATION | PRESENT STATUS | MATERIAL STUDIED |
|---|--|--|---|
| MACROSCALE | | | |
| Electron Mobility & Free Carrier Absorption | Practical determination of compensation ratio & total concentration of ionized impurities | Theory developed for n-type GaAs & InP & verified experimentally | n-type GaAs n-type InP |
| Transport in High Magnetic Field | Reliable determination of free carrier concen- tration & testing of sample homogeneity | Approach developed & verified experi- mentally | n-type GaAs n-type InP |
| MICROSCALE | | | |
| Scanning IR Absorption | Profiling of carrier concentration & ionized impurities | Apparatus completed, theory developed for n-type GaAs & InP | n, p-type Si (model experiments); n-type GaAs; n-type InP |
| SEM-Electron Beam-Induced Current | Instantaneous profiling of diffusion length, lifetime & surface recombination velocity | Apparatus completed, method developed & demonstrated | n, p-type Si (model experiments) n, p-type GaAs |

TRANSPORT IN HIGH MAGNETIC FIELD

Determination of carrier concentration from Hall-effect measurements involves ambiguity related to the value of the Hall factor, r , which in general can vary between 1.83 and 1, depending on the scattering properties of the semiconductor. However, in high-magnetic fields the Hall factor reduces to $r = 1$ independent of the nature of the scattering mechanism.

Accordingly, we have carried out Hall-effect measurements in magnetic fields up to 140 k Gauss for GaAs and InP samples. The results showed that for a number of samples the Hall constant vs. magnetic field exhibited anomalous behavior shown in Fig. 1; i.e., the Hall constant exhibited an increase, rather than the expected decrease with increasing magnetic field. Employing our scanning IR absorption technique, we have determined that this anomalous behavior is encountered only with the samples exhibiting carrier concentration inhomogeneities, $\Delta n/n_{av}$, exceeding about 20%. This finding, which agrees qualitatively with recent theoretical treatment of electron transport in inhomogeneous semiconductors, shows clearly that Hall measurements as a function of magnetic field provide a reliable means for the assessment of macroscopic homogeneity in InP and GaAs. It should also be noted that according to our findings about 80% of the studied melt-grown GaAs and InP samples (obtained from various suppliers) exhibited inhomogeneities exceeding 20%. Thus, standard, low-magnetic field Hall measurements, commonly used for the characterization of these materials, are totally unreliable.

SCANNING IR-ABSORPTION

Inhomogeneities in semiconducting materials are commonly recognized as constituting a limiting major factor in microelectronic device applications. Nevertheless, the quantitative determination of inhomogeneities on a micro-scale have been so far possible only in elemental semiconductors (Ge and Si).

The most commonly used method to obtain quantitative carrier distribution profiles is based on spreading resistance measurements. Pressure metal contacts, required for this technique, are highly irreproducible in the case of compound semiconductors, and the technique is not applicable to GaAs or InP characterization.

Accordingly, we have developed a method and constructed an apparatus for the contactless and nondestructive determination of the spatial variation of the free carrier concentration in III-V compounds which is, of course, applicable to other semiconductors. The method is based on the quantitative relationship between infrared absorption and free carrier concentration, and it is applicable to any semiconductor material with free carrier concentration exceeding 10^{15} cm^{-3} .

In this method a parallel beam from a CO_2 laser (tunable between 9.16 and 11.02 μm) is transmitted through the sample positioned on a stage with x-y motion and a scanning rate ranging from 50 to $10^{13} \mu\text{m}/\text{min}$. The light transmitted through the desired area of the sample is focused on a detector (bolometer) through the optics of an IR microscope; the signal from the detector, which is proportional to the intensity of radiation, is amplified and recorded; using a 74X objective the image of an area of about 20 μm in diameter is obtained.

The system permits a continuous monitoring of transmittance of the small wafer area, which is converted, through a data processing system, into variations of carrier concentration and of the compensation ratio. We have recently completed a rigorous theoretical treatment of the pertinent optical phenomena in n-type GaAs and InP required for the quantitative processing of the data. A typical microprofiling of InP obtained recently is given in Fig. 2. It is seen that a two-dimensional quantitative profile of the carrier concentration in InP single crystals has been achieved for the first time. This profile

clearly shows the pronounced inhomogeneities in the presently available melt-grown InP. Similar results have also been obtained with GaAs.

The spatial resolution of our IR-scanning system is about 20 μm and variations in the free carrier density in GaAs as low as $5 \times 10^{14} \text{ cm}^{-3}$ in n-type and $2.5 \times 10^{14} \text{ cm}^{-3}$ in p-type material can be detected.

Employing the same experimental system and a theoretical model we have developed we can determine in GaAs and InP the average value of the compensation ratio as well as its variations. It should be noted that this approach can be readily extended to any semiconductor.

SEM-ELECTRON BEAM-INDUCED CURRENT

In our approach scanning electron microscopy (SEM) is used primarily in the electron beam-induced current (EBIC) mode. Thus, the electron beam represents in essence a highly focused excitation source for excess minority carriers which are collected by a Schottky barrier or a p-n junction.

We have installed an SEM and accessory electronics especially designed for our EBIC mode approach. In parallel, we have been pursuing a theoretical and experimental study to advance our understanding of the excitation and recombination processes associated with the EBIC mode. In these studies we have used Si as a convenient model material, and we have obtained and confirmed high resolution profiles such as the minority carrier diffusion length, the lifetime, and in certain instances, the dopant profile. For the first time a direct correlation has been achieved on a microscale between compositional inhomogeneities and electronics parameters such as minority carrier diffusion length and lifetime.

We have utilized this technique to analyze diffusion length and the lifetime distribution in melt-grown and epitaxially grown GaAs. The results

provided direct evidence of out-diffusion of defects from substrate to epitaxially grown layers.

Extensive experimental work is in progress devoted to the extension of EBIC-mode technique to temperatures well below and well above room temperatures. In spite of inherent technical difficulties, we consider such an extension of key importance in identifying the specific mechanisms of minority carrier recombination which are the controlling factors in device performance.

TABLE 2

Electron Mobility, Carrier Concentration and Compensation Ratio
in n-type InP at 300 K

| Concen- tration | Compensation Ratio | | | | | | | | | | | | |
|----------------------|---|------|------|------|------|------|------|------|------|------|------|------|------|
| | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .75 | .80 | .85 | .90 | .95 |
| | Electron Mobility (cm^2/Vsec) | | | | | | | | | | | | |
| 1.0×10^{15} | 4710 | 4690 | 4660 | 4620 | 4570 | 4510 | 4410 | 4270 | 4160 | 4020 | 3820 | 3490 | 2900 |
| 1.5 | 4670 | 4630 | 4590 | 4540 | 4480 | 4390 | 4270 | 4090 | 3970 | 3800 | 3560 | 3210 | 2610 |
| 2 | 4640 | 4600 | 4550 | 4490 | 4410 | 4300 | 4160 | 3960 | 3810 | 3630 | 3380 | 3010 | 2420 |
| 3 | 4570 | 4510 | 4450 | 4370 | 4270 | 4140 | 3970 | 3730 | 3570 | 3360 | 3090 | 2720 | 2150 |
| 4 | 4520 | 4450 | 4370 | 4280 | 4160 | 4010 | 3820 | 3560 | 3380 | 3170 | 2900 | 2530 | 1980 |
| 5 | 4460 | 4390 | 4300 | 4190 | 4060 | 3900 | 3690 | 3410 | 3230 | 3020 | 2750 | 2380 | 1840 |
| 6 | 4420 | 4340 | 4240 | 4120 | 3980 | 3810 | 3590 | 3300 | 3120 | 2900 | 2620 | 2270 | 1740 |
| 7 | 4380 | 4290 | 4180 | 4060 | 3910 | 3730 | 3500 | 3200 | 3010 | 2790 | 2520 | 2170 | 1650 |
| 8 | 4330 | 4230 | 4120 | 3990 | 3830 | 3640 | 3410 | 3110 | 2920 | 2700 | 2440 | 2090 | 1570 |
| 9 | 4300 | 4200 | 4080 | 3940 | 3780 | 3580 | 3340 | 3030 | 2850 | 2630 | 2360 | 2020 | 1510 |
| 1.0×10^{16} | 4250 | 4140 | 4010 | 3870 | 3700 | 3500 | 3250 | 2950 | 2760 | 2550 | 2290 | 1950 | 1450 |
| 1.5 | 4080 | 3950 | 3800 | 3640 | 3460 | 3240 | 2990 | 2690 | 2500 | 2300 | 2044 | 1720 | 1240 |
| 2 | 3960 | 3820 | 3660 | 3480 | 3290 | 3070 | 2810 | 2510 | 2330 | 2120 | 1880 | 1560 | 1100 |
| 3 | 3770 | 3610 | 3440 | 3250 | 3050 | 2820 | 2570 | 2270 | 2100 | 1900 | 1660 | 1360 | 918 |
| 4 | 3630 | 3460 | 3280 | 3090 | 2880 | 2660 | 2400 | 2110 | 1940 | 1750 | 1510 | 1220 | 800 |
| 5 | 3530 | 3350 | 3170 | 2970 | 2770 | 2540 | 2290 | 2000 | 1830 | 1640 | 1410 | 1120 | 718 |
| 6 | 3440 | 3270 | 3080 | 2880 | 2670 | 2440 | 2190 | 1900 | 1740 | 1550 | 1320 | 1040 | 654 |
| 7 | 3370 | 3190 | 3000 | 2800 | 2590 | 2360 | 2120 | 1830 | 1660 | 1480 | 1250 | 973 | 604 |
| 8 | 3310 | 3130 | 2940 | 2730 | 2530 | 2300 | 2050 | 1770 | 1600 | 1410 | 1190 | 920 | 563 |
| 9 | 3260 | 3070 | 2880 | 2680 | 2470 | 2250 | 2000 | 1710 | 1550 | 1360 | 1140 | 875 | 530 |
| 1.0×10^{17} | 3220 | 3030 | 2830 | 2630 | 2420 | 2200 | 1950 | 1660 | 1500 | 1320 | 1100 | 835 | 501 |
| 1.5 | 3090 | 2900 | 2700 | 2490 | 2280 | 2060 | 1800 | 1520 | 1360 | 1180 | 970 | 723 | 423 |
| 2 | 2960 | 2760 | 2560 | 2350 | 2140 | 1910 | 1660 | 1370 | 1210 | 1040 | 839 | 611 | 345 |
| 3 | 2840 | 2640 | 2430 | 2210 | 1990 | 1750 | 1500 | 1220 | 1060 | 896 | 712 | 507 | 277 |
| 4 | 2770 | 2560 | 2340 | 2120 | 1890 | 1650 | 1400 | 1120 | 967 | 806 | 633 | 444 | 239 |
| 5 | 2720 | 2500 | 2270 | 2050 | 1820 | 1570 | 1320 | 1040 | 896 | 741 | 577 | 400 | 213 |
| 6 | 2680 | 2450 | 2220 | 1990 | 1760 | 1510 | 1260 | 987 | 844 | 694 | 536 | 369 | 194 |
| 7 | 2650 | 2410 | 2180 | 1940 | 1710 | 1460 | 1210 | 942 | 802 | 657 | 505 | 346 | 181 |
| 8 | 2620 | 2380 | 2140 | 1900 | 1660 | 1420 | 1160 | 900 | 764 | 623 | 477 | 325 | 169 |
| 9 | 2590 | 2350 | 2110 | 1860 | 1630 | 1380 | 1130 | 867 | 733 | 596 | 455 | 309 | 160 |
| 1.0×10^{18} | 2570 | 2320 | 2080 | 1830 | 1590 | 1350 | 1100 | 839 | 708 | 573 | 436 | 295 | 152 |
| 1.5 | 2470 | 2210 | 1960 | 1710 | 1460 | 1220 | 979 | 737 | 617 | 495 | 373 | 250 | 128 |
| 2 | 2390 | 2130 | 1870 | 1620 | 1380 | 1140 | 904 | 674 | 561 | 448 | 336 | 224 | 113 |
| 3 | 2290 | 2010 | 1750 | 1500 | 1260 | 1030 | 811 | 598 | 495 | 393 | 293 | 194 | 98 |
| 4 | 2210 | 1930 | 1670 | 1420 | 1190 | 965 | 755 | 553 | 456 | 361 | 268 | 177 | 89 |
| 5 | 2150 | 1880 | 1610 | 1360 | 1140 | 920 | 717 | 523 | 431 | 340 | 252 | 166 | 83 |
| 6 | 2100 | 1830 | 1560 | 1320 | 1100 | 886 | 687 | 501 | 411 | 325 | 241 | 158 | 79 |
| 7 | 2070 | 1790 | 1530 | 1290 | 1070 | 861 | 667 | 484 | 398 | 314 | 232 | 152 | 76 |
| 8 | 2040 | 1760 | 1500 | 1260 | 1040 | 838 | 647 | 470 | 386 | 304 | 225 | 148 | 74 |
| 9 | 2010 | 1740 | 1480 | 1240 | 1020 | 821 | 635 | 462 | 378 | 296 | 219 | 144 | 72 |
| 1.0×10^{19} | 1990 | 1710 | 1460 | 1230 | 1010 | 809 | 624 | 452 | 370 | 289 | 215 | 141 | 71 |

TABLE 3

Free Carrier Absorption in n-type InP
at 300 K, $m^* = 0.078$

| Concentration cm^{-3} | Free Carrier Absorption | | |
|-----------------------------------|-------------------------|----------------------|----------------------|
| | α_{imp} | α_{ac} | α_{op} |
| 1.0×10^{15} | | 0.003 | 0.058 |
| 1.5 | | 0.005 | 0.087 |
| 2 | 0.001 | 0.006 | 0.116 |
| 3 | | 0.010 | 0.174 |
| 4 | 0.001 | 0.013 | 0.231 |
| 5 | 0.001 | 0.016 | 0.289 |
| 6 | 0.001 | 0.019 | 0.346 |
| 7 | 0.002 | 0.022 | 0.404 |
| 8 | 0.002 | 0.025 | 0.461 |
| 9 | 0.003 | 0.029 | 0.518 |
| 1.0×10^{16} | 0.004 | 0.034 | 0.623 |
| 1.5 | 0.008 | 0.052 | 0.932 |
| 2 | 0.014 | 0.069 | 1.239 |
| 3 | 0.031 | 0.104 | 1.850 |
| 4 | 0.056 | 0.139 | 2.456 |
| 5 | 0.086 | 0.173 | 3.051 |
| 6 | 0.123 | 0.208 | 3.646 |
| 7 | 0.167 | 0.243 | 4.240 |
| 8 | 0.217 | 0.278 | 4.815 |
| 9 | 0.273 | 0.313 | 5.397 |
| 1.0×10^{17} | 0.314 | 0.325 | 5.578 |
| 1.5 | 0.690 | 0.491 | 8.227 |
| 2 | 1.201 | 0.660 | 10.79 |
| 3 | 2.602 | 1.005 | 15.75 |
| 4 | 4.474 | 1.360 | 20.52 |
| 5 | 6.790 | 1.726 | 25.16 |
| 6 | 9.510 | 2.100 | 29.65 |
| 7 | 12.64 | 2.488 | 34.11 |
| 8 | 16.13 | 2.879 | 38.44 |
| 9 | 20.00 | 3.285 | 42.75 |
| 1.0×10^{18} | 24.22 | 3.699 | 47.01 |
| 1.5 | 50.28 | 5.912 | 67.80 |
| 2 | 83.91 | 8.354 | 88.02 |
| 3 | 170.3 | 13.87 | 127.0 |
| 4 | 276.7 | 20.12 | 164.1 |
| 5 | 396.1 | 26.98 | 199.6 |
| 6 | 522.8 | 34.34 | 233.4 |
| 7 | 653.3 | 42.16 | 266.0 |
| 8 | 784.9 | 50.22 | 269.8 |
| 9 | 917.9 | 58.73 | 326.7 |
| 1.0×10^{19} | 1052 | 67.54 | 355.6 |

Compensation Ratio

| Concen- tration | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .75 | .8 | .85 | .9 | .95 |
|----------------------|---|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|-----------------------|----------------------|----------------------|-----------------------|
| | Electron Mobility (cm ² /Vsec) | | | | | | | | | | | | |
| 1.0x10 ¹³ | 3.06x10 ⁵ | 2.98x10 ⁵ | 2.88x10 ⁵ | 2.77x10 ⁵ | 2.63x10 ⁵ | 2.46x10 ⁵ | 2.25x10 ⁵ | 1.99x10 ⁵ | 1.83x10 ⁵ | 1.64x10 ⁵ | 1.42x10 ⁵ | 1.15x10 ⁵ | 8.01x10 ⁴ |
| 1.5 | 2.91 | 2.80 | 2.68 | 2.54 | 2.39 | 2.20 | 1.98 | 1.72 | 1.56 | 1.39 | 1.19 | 9.58x10 ⁴ | 6.64 |
| 2 | 2.77 | 2.65 | 2.52 | 2.37 | 2.20 | 2.01 | 1.79 | 1.53 | 1.39 | 1.23 | 1.05 | 8.41 | 5.78 |
| 3 | 2.56 | 2.42 | 2.27 | 2.11 | 1.94 | 1.74 | 1.53 | 1.30 | 1.17 | 1.03 | 0.87x10 ⁴ | 6.97 | 4.72 |
| 4 | 2.38 | 2.24 | 2.08 | 1.92 | 1.75 | 1.56 | 1.36 | 1.15 | 1.03 | 0.90x10 ⁴ | 7.68 | 6.09 | 4.05 |
| 5 | 2.25 | 2.09 | 1.94 | 1.77 | 1.61 | 1.43 | 1.24 | 1.04 | 0.93x10 ⁴ | 8.19 | 6.92 | 5.47 | 3.58 |
| 6 | 2.13 | 1.98 | 1.82 | 1.66 | 1.49 | 1.32 | 1.15 | 0.96x10 ⁴ | 8.60 | 7.54 | 6.36 | 5.00 | 3.22 |
| 7 | 2.03 | 1.87 | 1.72 | 1.56 | 1.40 | 1.24 | 1.07 | 0.86 | 8.02 | 7.02 | 5.91 | 4.62 | 2.94 |
| 8 | 1.92 | 1.77 | 1.62 | 1.47 | 1.31 | 1.16 | 1.00 | 0.83 | 7.47 | 6.52 | 5.48 | 4.26 | 2.68 |
| 9 | 1.87 | 1.71 | 1.56 | 1.41 | 1.26 | 1.11 | 0.96x10 ⁴ | 8.00 | 7.15 | 6.23 | 5.23 | 4.04 | 2.51 |
| 1.0x10 ¹⁴ | 1.80x10 ⁵ | 1.65x10 ⁵ | 1.50x10 ⁵ | 1.35x10 ⁵ | 1.21x10 ⁵ | 1.06x10 ⁵ | 9.16x10 ⁴ | 7.62x10 ⁴ | 6.81x10 ⁴ | 5.93x10 ⁴ | 4.96x10 ⁴ | 3.81x10 ⁴ | 2.35x10 ⁴ |
| 1.5 | 1.55 | 1.41 | 1.27 | 1.14 | 1.02 | 0.89x10 ⁴ | 7.65 | 6.33 | 5.61 | 4.87 | 4.02 | 3.03 | 1.80 |
| 2 | 1.38 | 1.25 | 1.13 | 1.01 | 0.97x10 ⁴ | 7.85 | 6.72 | 5.53 | 4.89 | 4.20 | 3.44 | 2.55 | 1.48 |
| 3 | 1.17 | 1.06 | 0.94x10 ⁴ | 8.46x10 ⁴ | 7.50 | 6.33 | 5.55 | 4.52 | 3.97 | 3.27 | 2.71 | 1.96 | 1.10 |
| 4 | 1.04 | 0.93x10 ⁴ | 8.39 | 7.47 | 6.60 | 5.72 | 4.84 | 3.90 | 3.40 | 2.86 | 2.27 | 1.62 | 0.95x10 ³ |
| 5 | 0.94x10 ⁴ | 8.30 | 7.60 | 6.75 | 5.95 | 5.14 | 4.32 | 3.45 | 2.99 | 2.50 | 1.97 | 1.39 | 0.758 |
| 6 | 0.876 | 7.86 | 7.02 | 6.22 | 5.47 | 4.71 | 3.93 | 3.12 | 2.69 | 2.34 | 1.75 | 1.23 | 0.62 |
| 7 | 0.821 | 7.36 | 6.56 | 5.80 | 5.09 | 4.36 | 3.63 | 2.86 | 2.46 | 2.03 | 1.58 | 1.10 | 0.591 |
| 8 | 0.774 | 6.93 | 6.17 | 5.44 | 4.76 | 4.07 | 3.37 | 2.64 | 2.26 | 1.86 | 1.44 | 1.00 | 0.533 |
| 9 | 0.736 | 6.58 | 5.85 | 5.15 | 4.49 | 3.83 | 3.16 | 2.46 | 2.10 | 1.72 | 1.33 | 0.90x10 ³ | 0.488 |
| 1.0x10 ¹⁵ | 7.04 | 6.29 | 5.58 | 4.91 | 4.27 | 3.63 | 2.98 | 2.31 | 1.97 | 1.61 | 1.24 | 0.853 | 0.51 |
| 1.5 | 5.87 | 5.22 | 4.60 | 4.01 | 3.46 | 2.90 | 2.35 | 1.80 | 1.52 | 1.23 | 0.93x10 ³ | 0.637 | 0.333 |
| 2 | 5.16 | 4.56 | 4.00 | 3.47 | 2.97 | 2.47 | 1.98 | 1.50 | 1.26 | 1.01 | 0.767 | 0.518 | 0.270 |
| 3 | 4.27 | 3.74 | 3.25 | 2.79 | 2.36 | 1.95 | 1.54 | 1.15 | 0.95x10 ³ | 0.767x10 ³ | 0.577 | 0.387 | 0.200 |
| 4 | 3.72 | 3.25 | 2.80 | 2.39 | 2.01 | 1.64 | 1.29 | 0.96x10 ³ | 0.793 | 0.632 | 0.474 | 0.317 | 0.163 |
| 5 | 3.33 | 2.89 | 2.48 | 2.11 | 1.76 | 1.43 | 1.12 | 0.824 | 0.682 | 0.542 | 0.405 | 0.271 | 0.139 |
| 6 | 3.05 | 2.64 | 2.26 | 1.90 | 1.59 | 1.28 | 1.00 | 0.734 | 0.606 | 0.481 | 0.359 | 0.239 | 0.123 |
| 7 | 2.82 | 2.43 | 2.07 | 1.74 | 1.45 | 1.17 | 0.90x10 ³ | 0.663 | 0.547 | 0.434 | 0.323 | 0.215 | 0.110 |
| 8 | 2.63 | 2.26 | 1.92 | 1.61 | 1.34 | 1.07 | 0.834 | 0.608 | 0.501 | 0.397 | 0.295 | 0.196 | 0.101 |
| 9 | 2.48 | 2.13 | 1.80 | 1.51 | 1.25 | 1.00 | 0.776 | 0.565 | 0.465 | 0.368 | 0.274 | 0.182 | 0.100x10 ² |
| 1.0x10 ¹⁶ | 2.35x10 ⁴ | 2.01x10 ⁴ | 1.70x10 ⁴ | 1.42x10 ⁴ | 1.17 | 0.93x10 ³ | 7.26x10 ³ | 5.28x10 ³ | 3.43x10 ³ | 3.43x10 ³ | 2.53x10 ³ | 1.70x10 ³ | 8.66x10 ² |
| 1.5 | 1.92 | 1.63 | 1.37 | 1.14 | 0.93x10 ³ | 7.42 | 5.70 | 4.12 | 3.38 | 2.67 | 1.98 | 1.31 | 0.67 |
| 2 | 1.67 | 1.41 | 1.18 | 0.97x10 ³ | 7.95 | 6.31 | 4.83 | 3.48 | 2.86 | 2.25 | 1.67 | 1.10 | 0.558 |
| 3 | 1.38 | 1.15 | 0.95x10 ³ | 7.86 | 6.39 | 5.05 | 3.86 | 2.77 | 2.27 | 1.78 | 1.32 | 0.93x10 ² | 0.438 |
| 4 | 1.20 | 1.00 | 0.830 | 6.81 | 5.52 | 4.36 | 3.32 | 2.38 | 1.95 | 1.53 | 1.13 | 0.742 | 0.373 |
| 5 | 1.08 | 0.90x10 ³ | 7.48 | 6.12 | 4.96 | 3.91 | 2.97 | 2.13 | 1.74 | 1.36 | 1.00 | 0.600 | 0.331 |
| 6 | 1.00 | 0.834 | 6.89 | 5.64 | 4.56 | 3.59 | 2.73 | 1.95 | 1.59 | 1.25 | 0.90x10 ² | 0.603 | 0.302 |
| 7 | 0.93x10 ³ | 7.79 | 6.43 | 5.25 | 4.24 | 3.34 | 2.53 | 1.81 | 1.48 | 1.16 | 0.853 | 0.558 | 0.279 |
| 8 | 0.868 | 7.22 | 5.96 | 4.87 | 3.94 | 3.10 | 2.36 | 1.69 | 1.38 | 1.08 | 0.799 | 0.524 | 0.262 |
| 9 | 0.844 | 7.02 | 5.78 | 4.72 | 3.81 | 2.99 | 2.27 | 1.62 | 1.32 | 1.03 | 0.759 | 0.497 | 0.248 |
| 1.0x10 ¹⁷ | 6.71 | 5.53 | 4.51 | 3.64 | 2.85 | 2.16 | 1.54 | 1.26 | 0.98x10 ² | 0.84x10 ² | 0.723 | 0.472 | 0.235 |
| 1.5 | 6.08 | 5.73 | 4.71 | 3.84 | 3.09 | 2.42 | 1.83 | 1.30 | 1.06 | 0.829 | 0.608 | 0.397 | 0.197 |
| 2 | 6.22 | 5.15 | 4.22 | 3.44 | 2.76 | 2.16 | 1.63 | 1.16 | 0.94x10 ² | 0.738 | 0.540 | 0.352 | 0.175 |
| 3 | 5.38 | 4.45 | 3.65 | 2.96 | 2.38 | 1.86 | 1.40 | 0.96x10 ² | 0.809 | 0.631 | 0.462 | 0.301 | 0.149 |
| 4 | 4.90 | 4.04 | 3.31 | 2.69 | 2.16 | 1.68 | 1.27 | 0.99 | 0.730 | 0.569 | 0.416 | 0.271 | 0.134 |
| 5 | 4.63 | 3.82 | 3.12 | 2.53 | 2.03 | 1.58 | 1.19 | 0.843 | 0.684 | 0.533 | 0.390 | 0.253 | 0.125 |
| 6 | 4.31 | 3.55 | 2.91 | 2.36 | 1.89 | 1.47 | 1.11 | 0.786 | 0.638 | 0.497 | 0.363 | 0.236 | 0.117 |
| 7 | 4.09 | 3.38 | 2.76 | 2.24 | 1.79 | 1.40 | 1.05 | 0.746 | 0.605 | 0.472 | 0.345 | 0.224 | 0.111 |
| 8 | 3.96 | 3.27 | 2.67 | 2.16 | 1.73 | 1.35 | 1.02 | 0.720 | 0.584 | 0.455 | 0.333 | 0.216 | 0.107 |
| 9 | 3.88 | 3.19 | 2.61 | 2.11 | 1.69 | 1.32 | 0.91x10 ² | 0.701 | 0.568 | 0.442 | 0.323 | 0.210 | 0.104 |
| 1.0x10 ¹⁸ | 3.74 | 3.07 | 2.51 | 2.04 | 1.63 | 1.27 | 0.957 | 0.678 | 0.548 | 0.428 | 0.312 | 0.203 | 0.101 |
| 1.5 | 3.37 | 2.79 | 2.26 | 1.83 | 1.47 | 1.14 | 0.861 | 0.612 | 0.498 | 0.385 | 0.281 | 0.182 | 0.090x10 ¹ |
| 2 | 3.71 | 2.61 | 2.12 | 1.72 | 1.38 | 1.09 | 0.802 | 0.579 | 0.464 | 0.363 | 0.264 | 0.167 | 0.080 |
| 3 | 2.70 | 2.37 | 2.00 | 1.68 | 1.34 | 0.91x10 ² | 0.751 | 0.533 | 0.434 | 0.336 | 0.236 | 0.159 | 0.0760 |

TABLE 4

Electron Mobility, Carrier Concentration and Compensation Ratio
in n-type InP at 77 K

TABLE 5

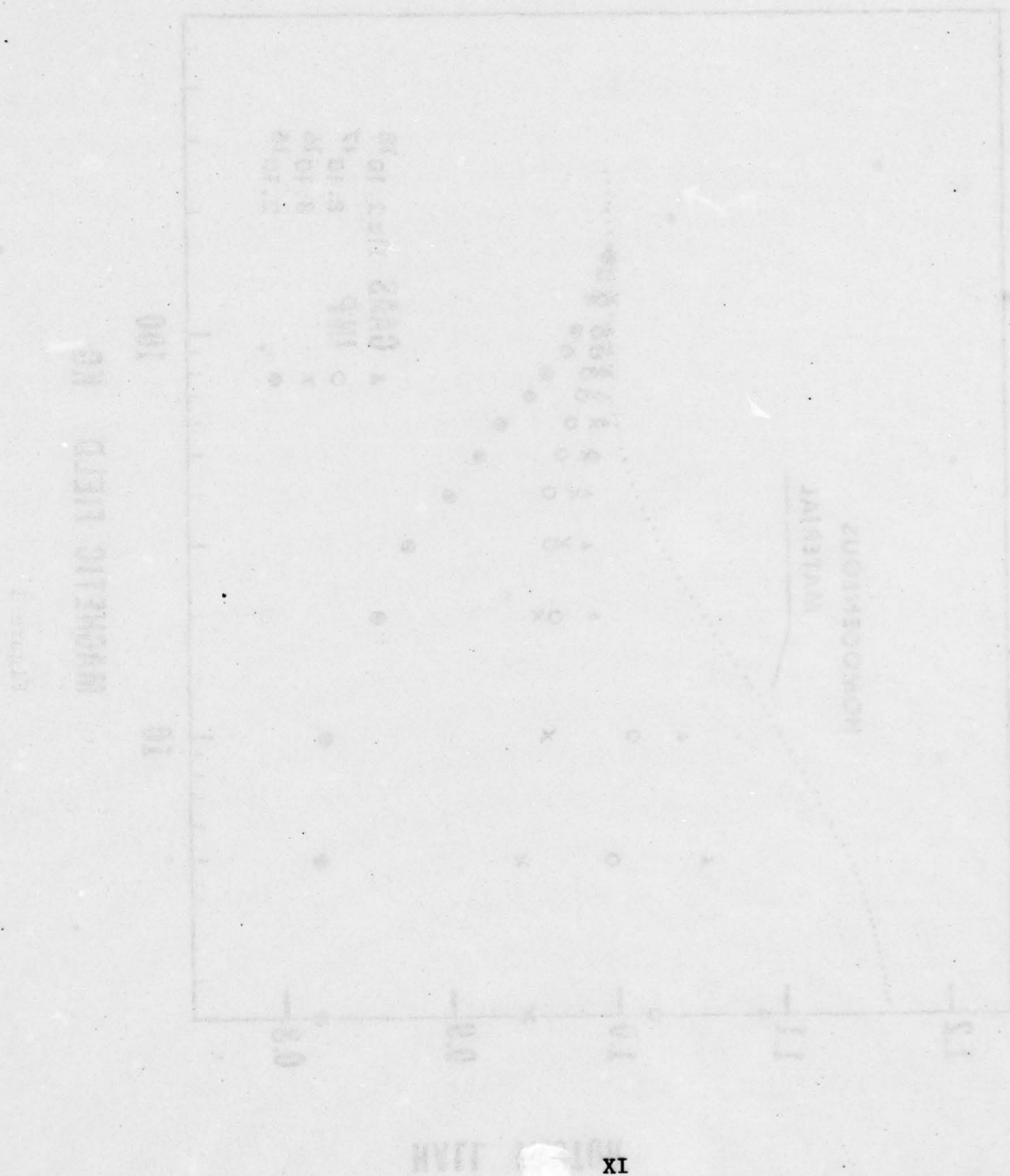
Free Carrier Absorption in n-type InP
at 77 K, $m^* = 0.082$

| Concentration cm^{-3} | Free Carrier Absorption | | |
|-----------------------------------|-------------------------|----------------------|----------------------|
| | α_{imp} | α_{ac} | α_{op} |
| 1.0×10^{15} | | 0.001 | 0.033 |
| 1.5 | | 0.001 | 0.049 |
| 2 | | 0.001 | 0.065 |
| 3 | | 0.002 | 0.097 |
| 4 | 0.001 | 0.002 | 0.130 |
| 5 | 0.001 | 0.003 | 0.162 |
| 6 | 0.001 | 0.003 | 0.194 |
| 7 | 0.002 | 0.004 | 0.225 |
| 8 | 0.002 | 0.004 | 0.257 |
| 9 | 0.003 | 0.005 | 0.289 |
| 1.0×10^{16} | 0.003 | 0.005 | 0.320 |
| 1.5 | 0.007 | 0.008 | 0.476 |
| 2 | 0.012 | 0.011 | 0.629 |
| 3 | 0.028 | 0.016 | 0.928 |
| 4 | 0.048 | 0.022 | 1.217 |
| 5 | 0.075 | 0.028 | 1.503 |
| 6 | 0.106 | 0.033 | 1.780 |
| 7 | 0.143 | 0.039 | 2.053 |
| 8 | 0.185 | 0.045 | 2.321 |
| 9 | 0.232 | 0.050 | 2.588 |
| 1.0×10^{17} | 0.284 | 0.056 | 2.849 |
| 1.5 | 0.617 | 0.086 | 4.127 |
| 2 | 1.066 | 0.117 | 5.366 |
| 3 | 2.296 | 0.181 | 7.793 |
| 4 | 3.949 | 0.250 | 10.19 |
| 5 | 6.009 | 0.322 | 12.60 |
| 6 | 8.460 | 0.398 | 15.02 |
| 7 | 11.27 | 0.476 | 17.41 |
| 8 | 14.49 | 0.560 | 19.90 |
| 9 | 18.05 | 0.646 | 22.38 |
| 1.0×10^{18} | 21.96 | 0.736 | 24.89 |
| 1.5 | 46.49 | 1.229 | 37.69 |
| 2 | 78.85 | 1.798 | 50.91 |
| 3 | 165.13 | 3.147 | 76.40 |
| 4 | 276.8 | 4.751 | 98.46 |
| 5 | 405.0 | 6.57 | 118.6 |
| 6 | 533.3 | 8.527 | 137.7 |

FIGURE CAPTIONS

Figure 1. Hall factor as a function of magnetic field.

Figure 2. Scanning IR absorption two-dimensional profile of n-type InP.



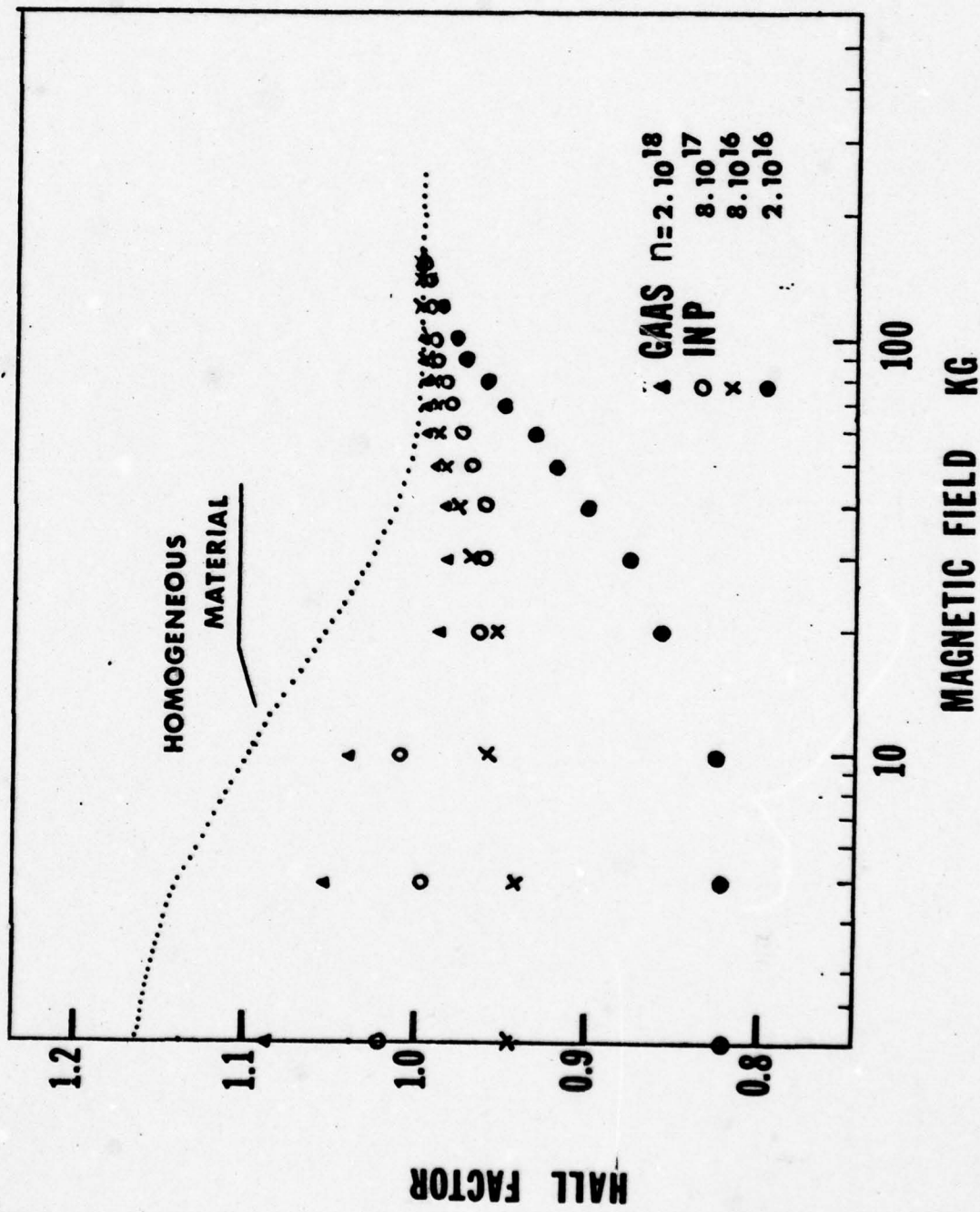


Figure 1

ELECTRON CONCENTRATION
| 5×10^{17} |

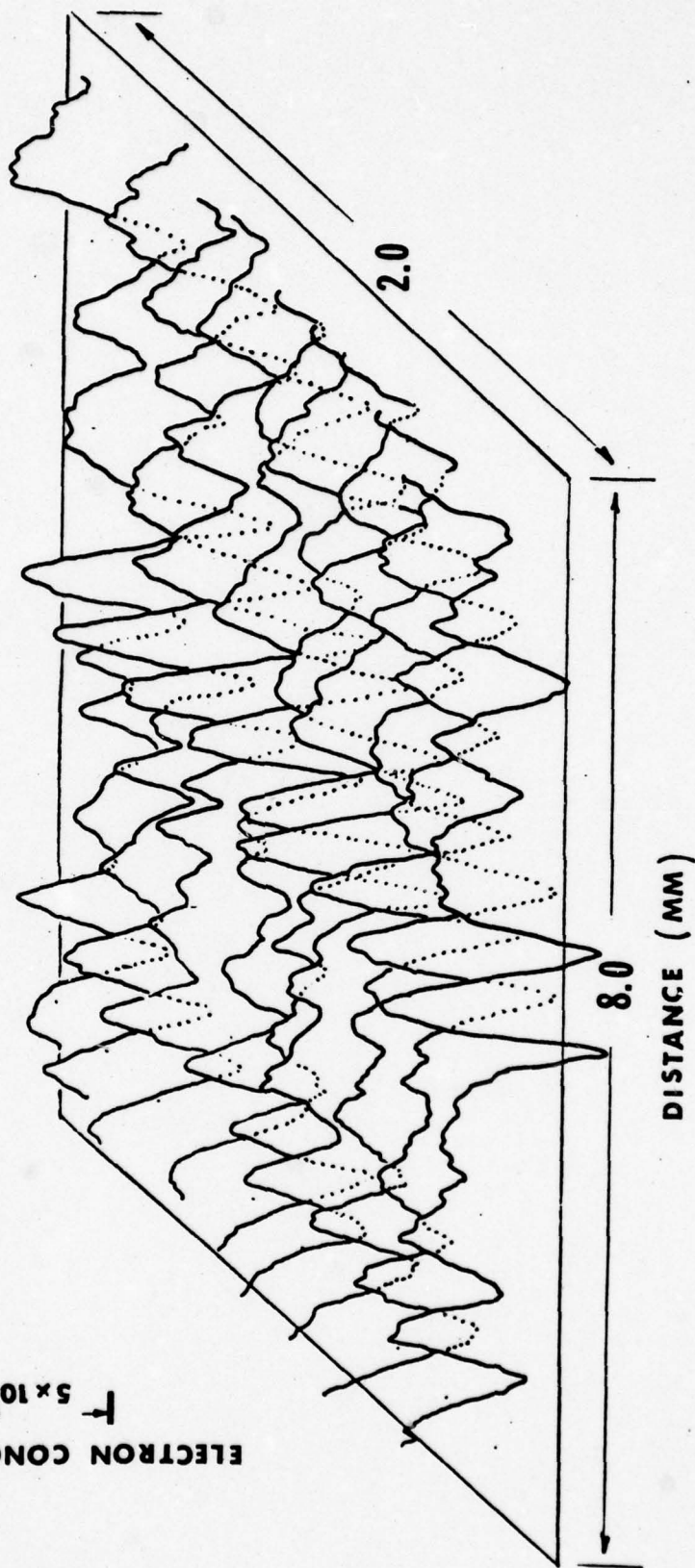


Figure 2

Appendix to Final Report on
ELECTRONIC CHARACTERISTICS OF
III-V COMPOUNDS

ELECTRON MOBILITY AND FREE CARRIER ABSORPTION IN GaAs;
DETERMINATION OF THE COMPENSATION RATIO

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ABSTRACT

Theoretical calculations of electron mobility and free carrier absorption in n-type GaAs at room temperature were carried out taking into consideration all major scattering processes. It was found that satisfactory agreement between theoretical and experimental results on free carrier absorption is obtained only when the effect of compensation is quantitatively taken into account. In conjunction with experimental studies it is shown that the electron mobility (for $n > 10^{15} \text{ cm}^{-3}$) and free carrier absorption (for $n > 10^{16} \text{ cm}^{-3}$) are sufficiently sensitive to the ionized impurity concentration to provide a

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reliable means for determining the compensation ratio.

Convenient procedures are presented for the determination of the compensation ratio from the free-carrier absorption coefficient and from the computed values of room temperature electron mobility. Values of the compensation ratio obtained by these two procedures are in good agreement provided the carrier concentration variations in the material are not appreciably greater than 10%

I. INTRODUCTION

III-V semiconductors usually exhibit an appreciable degree of compensation. Knowledge of the extent of compensation is important for the understanding of the basic electronic characteristics of these materials and their devices and for the evaluation of crystal growth processes. The methods for determining the compensation are usually related to the fact that the compensation reduces the free carrier concentration

and it enhances free carrier scattering by ionized impurities.

In GaAs, because of the small donor ionization energy (~ 5 meV), the accurate determination of donor and acceptor concentrations from free carrier concentration changes must be carried out at temperatures well below 15°K . Similarly, the determination of the compensation ratio from the amplitude of Schubnikov de Haas oscillations, as proposed recently,⁽¹⁾ must be carried out at 4.2°K . The low temperature requirements render these methods inaccessible for routine needs. Instead, methods based on scattering of free carriers by ionized impurities are employed. The reliable determination of the compensation ratio from free carrier scattering by ionized impurities is complicated, however, by the fact that longitudinal optical phonons contribute significantly to the overall scattering.⁽²⁾ For this polar mode scattering, the relaxation time cannot be defined except for low temperatures.⁽³⁾ Accordingly, it is necessary to use variational⁽⁴⁾ or iterative

procedures⁽²⁾ to combine all relevant scattering mechanisms.

Earlier approaches^(5, 6) to the determination of the compensation ratio from electron mobility neglected these aspects.

More recently, a rigorous semi-empirical procedure has been

formulated^(7, 8) for determining the compensation ratio in n-

type GaAs from the Hall constant and resistivity measurements

at 77°C. This procedure takes into consideration all major

scattering mechanisms but it is applicable only to nondegener-

ate material. Theoretical calculations of electron mobility

(based on an iterative procedure for solving the Boltzmann

equation) including compensation as a parameter and consider-

ing all major scattering mechanisms have also been reported.^(2, 9)

Although the screening of polar vibrations by free carriers

(which is significant at room temperature for $n > 10^{17} \text{ cm}^{-3}$)

was not taken into consideration, these results represent the

most reliable theoretical values of electron mobility in GaAs

thus far.

Free carrier absorption has been used also for the determination of the compensation ratio in n-type GaAs. (10-12)

In this approach (in contrast to that based on the electron mobility) the ionized impurity contribution to free carrier absorption is separable from contributions by other scattering mechanisms. This approach has not as yet been correlated with compensation ratio values obtained by other methods. Furthermore, the values of free carrier absorption available in the literature are not very reliable because the appropriate material parameters were not used in carrying out the computations. (13)

In the present study, the effect of compensation on two independently measured quantities, i.e., on the electron mobility and on the free carrier absorption, is considered. Theoretical computations of mobility are based on a variational method in the form proposed in ref (4) and they include all major scattering processes and screening effects. Computations

of the free carrier absorption coefficient are based on the approach of ref (10). A comparison is made with experimental results and with data available in the literature. (11, 15-18)

A procedure is outlined for the convenient determination of the compensation ratio from measured values of room temperature electron mobility and from the absorption coefficient at a wavelength of about $10\mu\text{m}$.

II. THEORY

A. General Considerations

The present theoretical calculations are intended to provide the basis for the determination of compensation ratio (or total density of ionized impurities) in n-type GaAs from independent room temperature measurements of the free carrier absorption and the electron mobility.

The electron mobility, μ , and the free carrier absorption coefficient, α , will be defined as:

$$\mu = \frac{\sigma(0)}{ne} ; \quad \alpha(\omega) = \frac{4\pi\sigma(\omega)}{cn_r} \quad (1)$$

where $\sigma(0)$ and $\sigma(\omega)$ are the dc and ac conductivity, respectively; n is the concentration of free electrons; c is the velocity of light and n_r is the refractive index at a given irradiation frequency, ω .

When the energy band structure, the electron-phonon coupling constants, and the electron concentration are known, the value of σ can be calculated if the total concentration of ionized impurities is also known. For n-type GaAs, the available material parameters are sufficiently accurate for a quantitative calculation of μ and $\alpha(\omega)$. For a given temperature, such calculations provide two absolute quantities, i.e., μ and $\alpha/\omega = \text{constant}$, and one functional dependence $\alpha(\omega)$, each of which can be used to determine the concentration of ionized impurities. Accordingly, in cases where ionized impurity scattering is appreciable, experimentally measured electron mobilities, free carrier absorption coefficients and the

frequency dependence of absorption coefficient can serve as the basis for testing the validity of the theoretical calculations and the reliability of the procedure for the determination of the compensation ratio.

In general, dc and ac conductivities can be treated in the same theoretical framework. In practice, however, it has been shown that dc conductivity is satisfactorily obtained from the solution of the semiclassical Boltzmann equation, (2, 4, 19) whereas ac conductivity can be conveniently obtained from second order perturbation theory. (10, 20-22) Both approaches are utilized in the present study; the computations are carried out using the material parameters given in Table (I) and discussed in detail in ref (2).

In view of the high (1.43 eV) and direct energy gap of GaAs, a single spherical, and parabolic conduction band described by an effective mass, m^* , will be assumed. With such an approximation, the electron mobility is slightly overestimated

and the free carrier absorption is underestimated. For this reason, an effective mass $m^*/m_0 = 0.068$ is used, which is somewhat higher than the exact value of the effective mass

$$m^*/m_0 = 0.064 \pm 0.002 \text{ at the band edge of GaAs.}^{(23)}$$

In the theoretical approach adopted in the present study, dilute solid solutions are assumed; i.e., interactions between impurities, quantum corrections for ionized impurity scattering⁽²⁴⁾ and differences in the short range part of the impurity potential are not taken into consideration. This assumption sets a limit to the electron (and impurity) concentration, which for n-type GaAs at room temperature can be realistically estimated to be $3 \times 10^{18} \text{ cm}^{-3}$. In this respect, it should be pointed out that differences in scattering by various impurities (Te, Se and S) in GaAs at concentrations above 10^{18} cm^{-3} have been indicated in refs (25, 16-18). However, a study of the electron mobility in about one thousand GaAs single crystals doped with Te, Se, Sn and Si has failed

to show any consistent differences among the various dopants;⁽²⁶⁾ the only difference (slightly lower mobility) was found in Si doped crystals (at concentrations exceeding 10^{18} cm^{-3}); this result was apparently due to the amphoteric behavior of Si.

B. Free Carrier Absorption

The present analysis will be confined to wavelengths greater than $4\mu\text{m}$, where transitions between various conduction band minima are negligible. Thus, only the lowest conduction band with a minimum at the center of the Brillouin zone (Γ_1) needs to be considered. The absorption of free carriers in a single conduction band constitutes an indirect transition in which momentum is conserved through interactions with the lattice. Using the approximation of a parabolic conduction band, the absorption coefficient can be directly calculated from the expressions derived in ref (10).

The total absorption coefficient α_t is

$$\alpha_t = \alpha_{op} + \alpha_{ac} + \alpha_{imp} \quad (2)$$

where α_{op} , α_{ac} and α_{imp} are the absorption coefficients corresponding to electron interactions with screened optical phonons, acoustic phonons and screened ionized impurities, respectively. Piezoelectric scattering is not taken into consideration; mobility calculations (see below) showed that for n-type GaAs, at room temperature the contribution of piezoelectric scattering to the total mobility is less than 2%; a similar contribution (which is within the accuracy of the calculations) is expected to the free carrier absorption.

According to ref (10), the absorption coefficients α_v can be written as follows where v designates op , ac or imp :

$$\alpha_v = \frac{C}{z^3} \int_0^\infty G_v(x, x'_v) \left\{ f(x) - f(x'_v) \right\} dx \quad (3)$$

where $f(x) = 1/(e^{x-\eta} + 1)$ is the electron distribution function; $x = E/k_0T$; $\eta = E_f/k_0T$ and $z = \hbar\omega/k_0T$ are the reduced electron energy, the Fermi energy and the incident photon energy,

respectively; k_0 is the Boltzmann constant and T is the absolute temperature. The values of C_v , G_v and x'_v are:

for optical phonons:

$$C_{op} = 2.96 \times 10^5 (m^*/m_0) \frac{z_l}{n_r} \left(\frac{1}{\epsilon_\infty} - \frac{1}{\epsilon_0} \right) \frac{\sinh(z/2)}{\sinh(z_l/2) \sinh(z'/2)} \quad (4)$$

$$G_{op} = 2P_{op} \left(1 + \frac{a^2}{D_{op}} \right) - aL_{op}; \quad x'_{op} = x + z \pm z_l$$

for ionized impurities:

$$C_{imp} = 2.175 \times 10^{-5} \frac{N_{imp}}{\epsilon_0^2 n_r T^2}; \quad G_{imp} = \frac{1}{4} L_{imp} - a \frac{P_{imp}}{D_{imp}} \quad (5)$$

$$x'_{imp} = x + z$$

for acoustic phonons:

$$C_{ac} = 4.79 \times 10^{11} (m^*/m_0)^2 \frac{TE_1^2}{n_r \rho v_l^2} \quad (6)$$

$$G_{ac} = P_{ac} B_{ac}$$

$$x'_{ac} = x + z$$

$$\text{where } P_v = (xx'_v)^{1/2}; \quad B_v = x + x'_v \quad (7)$$

$$L_v = \ln \frac{B_v + a + 2P_v}{B_v a - 2P_v}; \quad D_v = (B_v + a)^2 - 4P_v^2$$

The symbols in equations (4-7) are as follows:

ϵ_0 , ϵ_∞ are the static and the high frequency dielectric constants

$N_{\text{imp}} = N_D^+ + N_A^-$ is the concentration of ionized impurities

E_1 is the conduction band deformation potential

ρ is the crystal density

v_ℓ is the longitudinal sound velocity

$z_\ell = \frac{\hbar\omega_\ell}{k_0 T}$ is the reduced energy of longitudinal optical phonons

m_0 is the electron mass

a is the reduced screening energy:

$$a = \frac{\hbar^2}{2m^* \ell_D^2 k_0 T} \quad (8)$$

where the screening length ℓ_D is defined as

$$1/\ell_D^2 = 5.80 \times 10^{13} \frac{(m^*/m_0)^{3/2} T^{1/2}}{\epsilon_0} F_{-1/2}(\eta) \quad (9)$$

and $F_n(\eta)$ is the n-th order Fermi Dirac integral.

It should be noted that α_{op} is a sum of two terms given by

eq. (3) which correspond to $x'_{\text{op}} = x + z - z_\ell$ and $z' = z - z_\ell$

and to $x'_{op} = x + z + z_\ell$ and $z' = z + z_\ell$, respectively.

A discussion of the numerical calculations carried out on the basis of equations (2-9) and the GaAs parameters listed in Table (I) will be presented below together with experimental results.

The carrier concentration $n = N_D^+ - N_A^-$ (where N_D^+ and N_A^- are the concentrations of ionized donors and acceptors, respectively) enters into equations (2-9) through the reduced Fermi level η according to:

$$n = \frac{2}{\sqrt{\pi}} N_c F_{1/2}(\eta) \quad (10.1)$$

$$\text{or } n = 5.44 \times 10^{15} \left(\frac{m^*}{m_0} \right)^{3/2} \times F_{1/2}(\eta) \quad (10.2)$$

where N_c is the effective density of states in the conduction band.

The compensation ratio, θ , is defined as $\theta = N_A^- / N_D^+$; accordingly, the total concentration of the ionized impurities is related to the compensation ratio as follows:

$$N_{imp} = n \frac{1 + \theta}{1 - \theta} \quad (11)$$

It is apparent from eqs. (2-9) that for a given frequency of the incident light, and for a given electron concentration, only the term α_{imp} depends on the compensation ratio (being proportional to N_{imp}). Thus, if α_{exp} is the measured absorption coefficient in a material with a compensation ratio θ , and α_{op} , α_{ac} and α_{imp} are the absorption coefficients computed (from eqs. 3-9) for the same wavelength and the carrier concentration taking $\theta = 0$ (i.e., $N_{imp} = n$), the total concentration of ionized impurities can be determined as follows:

$$N_{imp} = n \frac{\alpha_{exp} - (\alpha_{op} + \alpha_{ac})}{\alpha_{imp}} \quad (12a)$$

which according to eq. (11) leads to the following expression for the compensation ratio:

$$\theta = \frac{\alpha_{exp} - (\alpha_{op} + \alpha_{ac})}{\alpha_{exp} + \alpha_{imp} - (\alpha_{op} + \alpha_{ac})} \quad (12b)$$

The values of α_{imp} , α_{op} and α_{ac} computed as a function of n for a wavelength of $10\mu m$ are given in Table (II).

A direct comparison between the experimental values of absorption coefficient and the theoretical dependence of the total free carrier absorption (computed from eqs. 2-7) on electron concentration is not possible, since samples with varying electron concentration can be characterized by a different degree of compensation. To provide a means for such comparison, a reduced experimental absorption coefficient, α_{exp}^* will be introduced representing α_{exp} for zero compensation.

$$\alpha_{\text{exp}}^* \equiv \alpha_{\text{exp}} - \frac{N_{\text{imp}}}{n} \alpha_{\text{imp}} \quad (13a)$$

which according to eq. (11) becomes

$$\alpha_{\text{exp}}^* = \alpha_{\text{exp}} - \alpha_{\text{imp}} \left(\frac{2\theta}{1 - \theta} \right) \quad (13b)$$

The theoretically obtained data in Table (II) can be used for relating α_{exp}^* to the compensation ratio as determined by other means (e.g., by electron mobility measurements). This procedure will be discussed below in conjunction with experimental results. At this time, an analytical extension of the above procedure to other wavelengths will be considered without

resorting to additional numerical calculations. In previous treatments (11, 20-22), approximate analytical expressions have been obtained on the frequency dependence of the absorption coefficient assuming a nondegenerate electron gas. They were found to be in fairly good agreement with experiment even in the case of highly doped materials for which the assumption of nondegeneracy is not satisfied. It can be shown, however, that these results are not inconsistent since similar analytical expressions can be obtained from eqs. (2-9).

Thus, in a spectral region, where:

$\hbar\omega$ is much greater than

$\hbar\omega_0$, E_F , $k_0 T$ and $ak_0 T$

eqs. (3-7) reduce to:

$$\alpha_{op} \approx \frac{4 C_{op}}{z^{2.5}} F_{1/2}(\eta) \quad \text{or} \quad \frac{\alpha_{op}}{n} = \frac{2\pi^{1/2}}{N_c} \left(\frac{k_0 T}{nC} \right)^{2.5} \times C_{op} \times \lambda^{2.5} \quad (14.1)$$

$$\alpha_{imp} \approx \frac{C_{imp}}{z^{3.5}} F_{1/2}(\eta) \quad \text{or} \quad \frac{\alpha_{imp}}{n} = \frac{\pi^{1/2}}{2N_c} \left(\frac{k_0 T}{nC} \right)^{3.5} \times \lambda^{3.5} \quad (14.2)$$

$$\alpha_{ac} \approx \frac{C_{ac}}{z^{1.5}} F_{1/2}(\eta) \quad \text{or} \quad \frac{\alpha_{ac}}{n} = \frac{\pi^{1/2}}{2N_c} \left(\frac{k_0 T}{nC} \right)^{1.5} \times C_{ac} \times \lambda^{1.5} \quad (14.3)$$

These expressions give the same frequency (or wavelength) dependence of the absorption coefficient as the expressions in refs (11, 20-22). For GaAs at room temperature and in the spectral region of 4-10 μ m inequality $\hbar\omega \gg \hbar\omega_0$, E_F , k_0T and ak_0T is fairly well satisfied up to an electron concentration of about 10^{18} cm^{-3} . For higher electron concentration eqs. (14.1-14.3) still constitute a reasonable approximation, for shorter wavelengths (e.g., 4-7 μ m), in agreement with previously reported experimental results. (11, 15)

According to eqs. (14.1-14.3), the procedure for determining the compensation ratio, from eq. (12), and the numerical values in Table (II) for $\lambda_0 = 10\mu\text{m}$, can be simply extended to other wavelengths λ , by calculating the absorption coefficient according to the approximate relationships:

$$\alpha_{\text{op}, \lambda_1} = \alpha_{\text{op}, \lambda_0} (\lambda_1/\lambda_0)^{2.5}; \quad (15)$$

$$\alpha_{\text{imp}, \lambda_1} = \alpha_{\text{imp}, \lambda_0} (\lambda_1/\lambda_0)^{3.5}$$

$$\alpha_{ac, \lambda_1} = \alpha_{ac, \lambda_0} (\lambda_1 / \lambda_0)^{1.5}$$

For an electron concentration $n = 10^{18} \text{ cm}^{-3}$ and for $8\mu\text{m} \leq \lambda \leq 12\mu\text{m}$ the error in absorption coefficients calculated according to eq. (15) (rather than from more exact numerical calculation based on eqs. (3-7)) does not exceed 9% for α_{imp} and 4% for $(\alpha_{op} + \alpha_{ac})$. These errors decrease rapidly with decreasing electron concentration.

C. Electron Mobility

The present computations of electron mobility are based on a variational principle method in the form proposed in ref (4, 19). This method allows to combine all scattering mechanisms without invoking the Matthiessen's rule, and it has been successfully applied to the calculation of mobilities in a number of semiconductor compounds. (3, 19, 27-30)

The following scattering mechanisms are considered:

screened optical phonon scattering, ⁽³¹⁾ screened ionized impurity scattering, ^(19, 32) acoustic phonon scattering through

the deformation potential⁽³³⁾ and piezoelectric interactions.⁽³⁴⁾

The final expression used (see Appendix I) is:

$$\mu = 308.6 \left[\left(\frac{1}{\epsilon^\infty} - \frac{1}{\epsilon_0} \right) \left(\frac{m^*}{m_0} \right)^{3/2} T^{1/2} z_\ell F_{1/2}(\eta) \right]^{-1} \times \frac{D_{3/2, 3/2}}{D} \quad (16)$$

where $D_{3/2, 3/2}$ and D are the determinants defined in the appendix.

Mobility values as a function of electron concentration obtained in the present study are shown in Fig. (1) together with results reported in ref (2) where an iterative procedure was used for solving the Boltzman equation; screening of polar scattering intentionally is not included in the calculations shown in Fig. (1) since this type of screening was not included in the calculations of ref (2). It is seen that the two methods are in very good agreement; the observed discrepancy at low and high electron concentration is primarily due to the assumption of a parabolic conduction band used in the present study; in ref (2) a nonparabolic conduction band was used with a slightly smaller band edge effective mass (0.066).

The component electron mobilities (i.e., electron mobilities calculated from eq. (16), for each scattering mechanism acting alone) are shown as a function of electron concentration in Fig. (2). It is seen that the maximum contribution to the total mobility from piezoelectric scattering does not exceed 2%, consistent with the assumption made above in the case of free carrier absorption. It is also seen that screening effects become pronounced for electron concentration exceeding 10^{17} cm^{-3} .

In Fig. 3 the total electron mobility calculated from eq. (16) is shown together with the electron mobility obtained by summarizing the component mobilities according to Matthiessen's rule (i.e., $1/\mu = \sum_i 1/\mu_i$). It is seen that for an electron concentration of 10^{17} cm^{-3} Mattheissen's rule leads to an error of about 30%. Thus, in determining the compensation ratio one must rely on the results of numerical calculations of mobility as a function of carrier concentration and compensation

ratio. The results obtained in the present study are summarized in Table (II).

III. COMPARISON WITH EXPERIMENT

A. Experimental Procedure and Sample Homogeneity

Hall effect, dc conductivity and infrared absorption measurements were carried out on n-type GaAs samples with electron concentrations ranging from 6×10^{15} to $2.6 \times 10^{18} \text{ cm}^{-3}$.

Melt-grown GaAs single crystals, obtained from commercial suppliers, and two epitaxially grown Te-doped layers (intentionally compensated with Ge) were used in this study. In order to obtain consistent and meaningful results, it was found necessary to assess the homogeneity of the samples. The carrier concentration distribution on a macro- and microscale was determined employing a recently reported IR scanning technique.⁽³⁵⁾ In the melt-grown commercial crystals, the spatial variation of the absorption coefficient, at $\lambda = 10.6 \mu\text{m}$ was found to be of the order of its average value (or Δn of

the order of n_{av}). In such samples the measured mobility can be higher⁽³⁶⁾ and the infrared absorption lower than theoretical limits. Accordingly, only samples with carrier concentration inhomogeneities not exceeding approximately 10% are considered in this study. The parameters of these samples are listed in Table (III).

The experimental values of the electron mobility and electron concentration were obtained from Hall-effect and conductivity measurements. In order to avoid ambiguities associated with the value of the Hall factor, r , the Hall constant was determined as a function of magnetic field up to a value of 100 KG; the saturation value (which corresponds to $r = 1$) was used to determine the electron concentration.

The results obtained are shown in Fig. (4) together with the theoretical dependence of electron mobility on electron concentration for different compensation ratios. The results of ref (18) which will be discussed below in conjunction

with free carrier absorption are also shown. It is seen that all mobility values are well below the theoretical values at zero compensation. From the electron concentration, and the electron mobility, the compensation ratio for each sample was determined directly from Table (II); the values of θ are given in Table (III). The normal range of mobility in commercially available high quality GaAs single crystals is indicated in Fig. (4) by the striped area; in the low electron concentration region, the available GaAs is significantly compensated and typically the total concentration of ionized impurities exceeds by an order of magnitude the electron concentration.

The absorption coefficient was determined from the transmittance, T , (measured with a Fourier spectrometer) using the expression:

$$T = \frac{(1-R)^2 e^{-\alpha d}}{1-R^2 e^{-2\alpha d}} \quad (17)$$

where d is the thickness of the sample and R is the

reflectance of GaAs (e.g., for $\lambda = 10\mu\text{m}$ $R = 0.28$), tabulated values of $R(\lambda)$ are given in ref (37). For sufficiently thin samples ($ad < 1$) the transmittance measured as a function of the thickness of the sample can also be used to determine $R(\lambda)$. Measurements carried out in this study showed that for electron concentrations exceeding 10^{18} cm^{-3} and for $\lambda > 10\mu\text{m}$ the reflectance decreases with increasing electron concentration (see also refs 12, 15). However, for lower electron concentrations, R was found to be essentially independent of n .

The transmission measurements, intended to provide a basis for determining the absorption coefficient, were carried out on thick samples and with the exception of sample No. 7, the condition $ad > 1$ was satisfied for wavelengths in the vicinity of $10\mu\text{m}$.

The experimental results on the absorption coefficient for $\lambda = 10\mu\text{m}$ are given in Fig. (5) together with those available in the literature. For comparison, the theoretical values of

the total absorption coefficient α_t and the absorption components α_{op} , α_{imp} and α_{ac} are also given in Fig. (V). As it has been discussed above, these absorption coefficients were computed assuming no compensation. Thus, it is understandable that the experimental values of α are greater than the theoretical ones. Some of the experimental values of ref (11) are smaller than those computed theoretically. Although the reason for this discrepancy is not clear, it should be noted that in the present study absorption coefficients smaller than those obtained theoretically were observed in samples exhibiting significant carrier concentration inhomogeneities.

B. Characteristics of Free Carrier Absorption

As pointed out above, a comparison between the experimental and theoretical dependence of free carrier absorption on the electron concentration for samples of different degrees of compensation can be achieved by reducing the experimental absorption coefficient to zero compensation (eq. 13b).

Such a reduction of the experimental results of Fig. (5) was carried out using the values of compensation ratio determined for each sample from electron mobility (Table III), and the computed values of α_{imp} as given in Table (II). The results of α_{exp}^* vs. electron concentration are given in Fig. (6) together with the theoretical dependence of $\alpha_t(n)$. The obtained agreement is very good, and it is worth emphasizing that no adjustable parameters were used in calculation of the mobility, which provides the basis for determination of θ , and of the free carrier absorption coefficient.

The values of the compensation ratio determined from electron mobilities (Table III) have also been used to compare the experimental and theoretical dependence of the absorption coefficient on the wavelength λ . Typical results are given in Fig. (7). It is seen that very good agreement is obtained when the effect of compensation is quantitatively taken into account. It is also seen that for the lower electron

concentration ($n = 1.1 \times 10^{17} \text{ cm}^{-3}$) the compensation affects noticeably both the absolute value of α and its wavelength dependence (i.e., the slope $d\ln\alpha/d\ln\lambda$). This behavior is not surprising since, with increasing compensation, the dominant role of polar scattering is superseded by ionized impurity scattering. These two scattering modes lead to different wavelength dependences of the absorption coefficient.

C. Compensation Ratio

The present results have shown that the measured values of electron mobility (Table III) and the experimental characteristics of the free carrier absorption (concentration and wavelength dependences) are satisfactorily explained by theory taking into account compensation.

As discussed above, the value of the compensation ratio can be determined independently from the electron mobility and the electron concentration (utilizing Table II) and from the free

carrier absorption coefficient (utilizing eq. 12b, and the values of absorption components given in Table II). The values of θ obtained by these methods are in very good agreement as shown in Table (III). The differences in values of θ are within experimental error which is primarily due to inhomogeneity of the material. In the case of intentionally compensated epitaxial layers (4 and 5 in Table III), the values of θ determined (0.67 and 0.76, respectively) here are in good agreement with the nominal compensation ratio estimated from the concentration of impurities introduced during the growth (i.e., 0.7 and 0.75, respectively). Thus, it must be concluded that both procedures for determining the compensation ratio lead to reliable and consistent results.

As pointed out above, the upper limit to which the present approach is applicable corresponds to electron (and impurity) concentrations of about $3 \times 10^{18} \text{ cm}^{-3}$. The lower concentration limit is determined by the sensitivity of the room

temperature electron mobility and of the free carrier absorption to ionized impurities. These limits are apparent from Table (II) (and/or Figs. 4 and 5). Thus, for a reliable determination of the compensation ratio from electron mobility, the electron concentration should be greater than 10^{15} cm^{-3} , and in the case of free carrier absorption, the electron concentration should be greater than 10^{16} cm^{-3}). It should also be emphasized that, for the reliable application of the present procedures, GaAs should be reasonably homogeneous. Thus, it is desirable to supplement measurements of mobility and/or free carrier absorption with measurements of the carrier concentration distribution on a microscale. Employing scanning IR absorption⁽³⁵⁾ for this purpose, it also becomes possible (on the basis of the present study) to obtain a compensation ratio profile with a spatial resolution of about $20 \mu\text{m}$.

SUMMARY

Theoretical and experimental studies of room temperature

electron mobility and free carrier absorption coefficient have been carried out on n-type GaAs. It was shown that for a total concentration of ionized impurities smaller than 10^{15} cm^{-3} , the room temperature electron mobility is dominated by polar scattering (with about 10% contribution from acoustic phonon and piezoelectric scattering) and it approaches a value of about $8000 \text{ cm}^2/\text{Vsec}$, in agreement with previous experimental and theoretical results. For impurity concentrations exceeding 10^{15} cm^{-3} , the mobility becomes sensitive to ionized impurity scattering permitting the determination of the compensation ratio in the material. It was found, however, that the contribution from ionized impurity cannot be analytically separated from other scattering mechanisms since the application of Matthiessen's rule leads to significant errors. Thus, in determining the compensation ratio, one must rely on the results of numerical calculations. The calculated values of electron mobility as a function of compensation ratio given in Table (II)

can be readily used for the determination of the compensation ratio in n-type GaAs with electron concentrations ranging from 10^{15} to $3 \times 10^{18} \text{ cm}^{-3}$.

It was also shown that the free carrier absorption coefficient is sensitive to compensation in GaAs for electron concentrations exceeding 10^{16} cm^{-3} . An analysis of the present experimental results and those available in the literature showed that the characteristics of free carrier absorption (concentration and wavelength dependences) can be satisfactorily explained only when compensation is quantitatively accounted for.

A procedure for the determination of the compensation ratio from the value of free carrier absorption coefficient for $\lambda_0 = 10 \mu\text{m}$ (or other wavelengths $8 \mu\text{m} \leq \lambda \leq 12 \mu\text{m}$), and the calculated values of the component absorption coefficients was outlined. For reasonably homogeneous materials, a good agreement was obtained between the values of compensation ratios

obtained from electron mobility and from free carrier absorption. It should be pointed out, that no fitting parameters other than the compensation ratio were used in comparing the experimental and theoretical results.

It was thus concluded that both the room temperature electron mobility and the free carrier absorption coefficient provide a reliable and consistent means for determining the degree of compensation (or the total concentration of ionized impurities) in n-type GaAs. In the form presented here, these methods can be used as practical procedures requiring relatively simple instrumentation. The electron concentration and mobility can be determined by means of standard conductivity and Hall effect measurements, taking the Hall factor r as unity; the error due to this assumption is estimated to be about 10% for $n \approx 10^{15} \text{ cm}^{-3}$ and decreases with increasing carrier concentration.

The free carrier absorption method outlined here

requires the determination of the absorption coefficient for one arbitrarily chosen wavelength in the spectral region $8\mu\text{m} \leq \lambda \leq 12\mu\text{m}$. Accordingly, relatively simple IR spectrometric instrumentation is required (e.g., a CO_2 laser and suitable IR detector). For sufficiently thick samples (satisfying the condition $ad \geq 1$) the error associated with minor changes in reflectance due to electron concentration changes can be neglected (for $n \leq 3 \times 10^{18} \text{ cm}^{-3}$) and one can utilize the values of $R(\lambda)$ given in ref (36). When the electron concentration, the electron mobility and/or the free carrier absorption coefficient are experimentally determined, the compensation ratio and the total number of ionized impurities can be determined from Table (II) and eqs. (11) or (12).

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APPENDIX

Equation (16) describing low field electron mobility has been obtained with the aid of the variational principle method⁽⁴⁾ adapted to the case of the screened electron-optical phonon interaction.⁽²⁷⁾ The change of the electron distribution function, f , can be written in the form:

$$\left(\frac{\partial f}{\partial t} \right)_{\text{coll}} = - Ak \cos \phi \frac{\partial f}{\partial x} L(C) \quad (\text{A.1})$$

where $x = \frac{E}{k_0 T}$; E is the electron energy, $k \cos \phi$ is the projection of the electron wave vector on the electric field

direction and

$$A = A(x, T, m_o^*) = 4.768 \times 10^{28} \frac{z_l}{x^{3/2}} \frac{(m^*/m_o)^{1/2}}{T^{1/2}} \left(\frac{1}{\epsilon_\infty} - \frac{1}{\epsilon_o} \right) \quad (\text{A.2})$$

Operator $L(C)$ consists of four terms describing the different scattering mechanisms considered at present

$$L(C) = L_{\text{opt}}(C) + \frac{C(E)}{A} \left[\frac{1}{\tau_{\text{imp}}} + \frac{1}{\tau_{\text{ac}}} + \frac{1}{\tau_{\text{pel}}} \right] \quad (\text{A.3})$$

The relaxation times, τ , for elastic scattering processes are

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given by,

screened ionized impurities: (32)

$$\frac{1}{\tau_{\text{imp}}} = 2.415 \frac{N_{\text{imp}}}{\epsilon_0} \left(\frac{m^*}{m_0} \right)^{-1/2} (xT)^{-3/2} \left[\ln \left(1 + \frac{4x}{a} \right) - \frac{\frac{4x}{a}}{1 + \frac{4x}{a}} \right] \quad (\text{A.4})$$

acoustic phonon scattering through deformation

potential: (33)

$$\frac{1}{\tau_{\text{ac}}} = 4.167 \times 10^{19} \frac{E_1^2}{\rho v_\ell^2} \left(\frac{m^*}{m_0} T \right)^{3/2} x^{1/2} \quad (\text{A.5})$$

piezoelectric (acoustic mode) scattering: (34)

$$\frac{1}{\tau_{\text{pel}}} = 1.052 \times 10^7 \times h_{14}^2 \left(\frac{3}{C_\ell} + \frac{4}{C_t} \right) \left(\frac{T}{x} \frac{m^*}{m_0} \right)^{1/2} \quad (\text{A.6})$$

For screened optical phonon (polar) scattering: (27)

$$\begin{aligned} L_{\text{opt}}(C) = & \frac{f_+}{f} (N+1) C_+ \left[(R_+ + a) S_+ - a R_+ T_+ - 4U_+ \right] \\ & - 2x \frac{f_+}{f} (N+1) C_+ \left[S_+ - a T_+ \right] + h(x - z_\ell) \left\{ \frac{N f_-}{f} C_- \right. \\ & \left. \left[(R_- + a) S_- - a R_- T_- - 4U_- \right] - 2x N C_- \frac{t_-}{f} \left[S_- - a T_- \right] \right\} \quad (\text{A.7}) \end{aligned}$$

where $f_\pm = f_0 (x \pm z_\ell)$; $C_\pm = C (E \pm \hbar \omega_\ell)$

$$R_\pm = 2x + a \pm z_\ell; U_\pm = \sqrt{x(x \pm z_\ell)}$$

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$$T_{\pm} = \frac{4U_{\pm}}{R_{\pm}^2 - 4U_{\pm}^2} ; S_{\pm} = \ln \left[\frac{R_{\pm} + 2U_{\pm}}{R_{\pm} - 2U_{\pm}} \right]$$

and $N = \frac{1}{e^{z_{\ell}} - 1}$ is the optical phonon occupation number.

Following the procedure developed in ref (4), one obtains the following expression for electron mobility:

$$\mu = 308.6 \left[\left(\frac{1}{\epsilon_{\infty}} - \frac{1}{\epsilon_0} \right) \left(\frac{m^*}{m_0} \right)^{3/2} T^{1/2} z_{\ell} F_{1/2}(n) \right]^{-1} \frac{D_{3/2, 3/2}}{D} \quad (A.8)$$

where the determinants have forms

$$D_{3/2, 3/2} = \begin{vmatrix} 0 & \beta_0^{(3/2)} & \beta_1^{(3/2)} & \dots \\ \beta_0^{(3/2)} & d_{00} & d_{01} & \dots \\ \beta_1^{(3/2)} & d_{10} & d_{11} & \dots \\ \cdot & \cdot & \cdot & \\ \cdot & \cdot & \cdot & \\ \cdot & \cdot & \cdot & \end{vmatrix} \quad (A.9)$$

$$D = \begin{vmatrix} d_{00} & d_{01} & \dots \\ d_{10} & d_{11} & \dots \\ \cdot & \cdot & \\ \cdot & \cdot & \\ \cdot & \cdot & \end{vmatrix} \quad (A.10)$$

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The elements of the determinants are given by the integrals:

$$\beta_r^{(3/2)} = \int_0^\infty E^{3/2} \phi_r \frac{\partial f_0}{\partial E} dE \quad (\text{A.11})$$

$$d_{r,s} = \int_0^\infty \phi_r L(\phi_s) \frac{\partial f_0}{\partial E} dE \quad (\text{A.12})$$

The functions ϕ_r should represent a complete set of functions of electron energy E . In the present computations, the set $\phi_{r(s)} = E^{r(s)}$ was chosen with values of r and s equal to 0, 1 and 2, which at room temperature assure an accuracy of the mobility calculations within a few percent. (4, 38)

TABLE I

GaAs parameters used in present computations (300° K)
(after refs 2 and 9)

low frequency

dielectric constant, ϵ_0 12.91

high frequency

dielectric constant, ϵ_∞ 10.91

optical phonon

energy, $\hbar\omega_0$ 36 meV

deformation

potential, E_1 7 eV

longitudinal

elastic constant, $C_\ell = \rho v_\ell^2$ 14.03×10^{11} dyne/cm²

piezoelectric

coefficient, $h_{14}^2 \left(\frac{3}{C_\ell} + \frac{4}{C_t} \right)$ 2.39×10^{-2}

effective mass, m^*/m_0

0.068 (see text)

TABLE II

Computed Values of Electron Mobility and IR Absorption in n-type GaAs

| CONCENTRATION | COMPENSATION RATIO | ELECTRON MOBILITY (cm^2/Vsec) | | | | | | | | | | ABSORPTION at $10\mu\text{m}$ (cm^{-1}) | | |
|---------------|-----------------------|---|------|------|------|------|------|------|------|------|------|--|----------------------|----------------------|
| | | .0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | α_{imp} | α_{ac} | α_{op} |
| | | | | | | | | | | | | | | |
| | 1×10^{15} | 7810 | 7760 | 7700 | 7620 | 7530 | 7400 | 7220 | 6940 | 6490 | 5590 | | | |
| | 1.5 | 7740 | 7680 | 7590 | 7490 | 7360 | 7200 | 6970 | 6640 | 6120 | 5150 | | | |
| | 2 | 7600 | 7510 | 7410 | 7290 | 7140 | 6950 | 6690 | 6330 | 5770 | 4780 | | | |
| | 3 | 7540 | 7430 | 7300 | 7150 | 6960 | 6730 | 6420 | 6000 | 5400 | 4370 | | | |
| | 4 | 7450 | 7320 | 7170 | 6990 | 6780 | 6510 | 6180 | 5730 | 5100 | 4070 | | | |
| | 5 | 7370 | 7230 | 7060 | 6870 | 6640 | 6350 | 6000 | 5540 | 4850 | 3870 | | | |
| | 6 | 7280 | 7130 | 6950 | 6730 | 6490 | 6190 | 5820 | 5340 | 4700 | 3670 | | | |
| | 7 | 7230 | 7060 | 6860 | 6640 | 6380 | 6060 | 5680 | 5200 | 4540 | 3510 | | | |
| | 8 | 7150 | 6970 | 6760 | 6530 | 6260 | 5930 | 5540 | 5050 | 4390 | 3370 | | | |
| | 9 | 7050 | 6860 | 6650 | 6400 | 6120 | 5790 | 5390 | 4900 | 4250 | 3232 | | | |
| | 1×10^{16} | 6980 | 6790 | 6560 | 6310 | 6020 | 5680 | 5280 | 4790 | 4140 | 3120 | .0036 | .025 | .341 |
| | 1.5 | 6710 | 6480 | 6230 | 5950 | 5640 | 5280 | 4870 | 4370 | 3720 | 2710 | .0080 | .038 | .510 |
| | 2 | 6500 | 6250 | 5980 | 5680 | 5360 | 5000 | 4580 | 4080 | 3430 | 2440 | .0142 | .050 | .679 |
| | 3 | 6190 | 5920 | 5630 | 5320 | 4980 | 4610 | 4180 | 3680 | 3030 | 2060 | .032 | .075 | 1.01 |
| | 4 | 5970 | 5690 | 5380 | 5060 | 4720 | 4340 | 3910 | 3410 | 2760 | 1820 | .056 | .100 | 1.35 |
| | 5 | 5810 | 5510 | 5200 | 4870 | 4520 | 4140 | 3710 | 3200 | 2560 | 1640 | .087 | .126 | 1.68 |
| | 6 | 5680 | 5370 | 5050 | 4720 | 4370 | 3980 | 3550 | 3040 | 2400 | 1510 | .125 | .152 | 2.00 |
| | 7 | 5570 | 5260 | 4940 | 4600 | 4250 | 3860 | 3420 | 2910 | 2270 | 1400 | .169 | .178 | 2.32 |
| | 8 | 5480 | 5160 | 4840 | 4490 | 4140 | 3740 | 3300 | 2790 | 2160 | 1320 | .220 | .203 | 2.65 |
| | 9 | 5400 | 5080 | 4750 | 4400 | 4040 | 3640 | 3200 | 2690 | 2060 | 1240 | .277 | .229 | 2.97 |
| | 1×10^{17} | 5330 | 5010 | 4670 | 4320 | 3960 | 3560 | 3120 | 2600 | 1980 | 1180 | .340 | .255 | 3.28 |
| | 1.5 | 5090 | 4750 | 4400 | 4030 | 3650 | 3240 | 2790 | 2280 | 1690 | 960 | .746 | .387 | 4.84 |
| | 2 | 4910 | 4540 | 4160 | 3780 | 3390 | 2970 | 2520 | 2030 | 1470 | 820 | 1.29 | .521 | 6.35 |
| | 3 | 4730 | 4350 | 3960 | 3560 | 3160 | 2730 | 2280 | 1790 | 1270 | 680 | 2.79 | .796 | 9.26 |
| | 4 | 4530 | 4130 | 3730 | 3320 | 2920 | 2490 | 2050 | 1590 | 1100 | 580 | 4.82 | 1.08 | 12.1 |
| | 5 | 4470 | 4060 | 3640 | 3220 | 2800 | 2380 | 1940 | 1490 | 1020 | 530 | 7.26 | 1.34 | 14.8 |
| | 6 | 4370 | 3950 | 3520 | 3100 | 2680 | 2260 | 1830 | 1390 | 950 | 480 | 10.2 | 1.68 | 17.5 |
| | 7 | 4290 | 3860 | 3420 | 3000 | 2580 | 2160 | 1740 | 1320 | 890 | 450 | 13.5 | 1.99 | 20.1 |
| | 8 | 4220 | 3780 | 3340 | 2910 | 2500 | 2080 | 1670 | 1260 | 840 | 420 | 17.2 | 2.32 | 22.7 |
| | 9 | 4160 | 3710 | 3270 | 2840 | 2430 | 2010 | 1610 | 1200 | 800 | 400 | 21.3 | 2.65 | 25.3 |
| | 1×10^{18} | 4100 | 3640 | 3200 | 2770 | 2360 | 1950 | 1550 | 1160 | 770 | 380 | 25.8 | 3.00 | 27.9 |
| | 1.5 | 3860 | 3400 | 2950 | 2520 | 2130 | 1740 | 1370 | 1010 | 660 | 330 | 53.4 | 4.85 | 40.5 |
| | 2 | 3690 | 3220 | 2780 | 2360 | 1980 | 1600 | 1250 | 920 | 600 | 290 | 88.8 | 6.91 | 52.8 |
| | 3 | 3460 | 3000 | 2560 | 2160 | 1790 | 1440 | 1120 | 810 | 530 | 260 | 178 | 11.6 | 76.6 |
| | 4 | 3300 | 2840 | 2410 | 2020 | 1670 | 1340 | 1040 | 750 | 480 | 230 | 284 | 16.9 | 98.6 |
| | 5 | 3200 | 2750 | 2330 | 1950 | 1600 | 1280 | 990 | 710 | 460 | 220 | 400 | 22.8 | 120 |

TABLE III

Compensation Ratios Derived from Mobility and IR Absorption Measurements

| SAMPLE NO. | ELECTRON CONCENTRATION (cm^{-3}) | GROWTH | DOPANT | HOMOGENEITY $\Delta n/n_{av}$ | MOBILITY cm^2/Vsec | COMPENSATION RATIO, θ | MOBILITY | ABSORPTION |
|------------|---|--------|--------|----------------------------------|---------------------------------------|------------------------------|----------|-----------------|
| 1. | 3×10^{16} | melt | Te | $\leq 10\%$ | 2700 | 0.83 ± 0.03 | | 0.89 ± 0.05 |
| 2. | 1.1×10^{17} | melt | ? | $\leq 10\%$ | 1800 | 0.83 ± 0.03 | | 0.85 ± 0.03 |
| 3. | 5.5×10^{17} | melt | Te | $\leq 10\%$ | 3300 | 0.25 ± 0.06 | | 0.23 ± 0.08 |
| 4.* | 8.5×10^{17} | LPE | Te | $\leq 3\%$ | 1350 | 0.67 ± 0.03 | | 0.65 ± 0.04 |
| 5.* | 1.5×10^{18} | LPE | Te | $\leq 3\%$ | 800 | 0.76 ± 0.02 | | 0.77 ± 0.03 |
| 6. | 2.0×10^{18} | melt | ? | $\leq 15\%$ | 2100 | 0.37 ± 0.08 | | 0.29 ± 0.08 |
| 7. | 6×10^{15} | melt | -- | $\leq 20\%$ | 3300 | $> .9$ | | $> .9$ |
| 8. | 2.6×10^{18} | melt | -- | $\leq 20\%$ | 1650 | 0.40 ± 0.1 | | 0.3 ± 0.1 |
| Ref (18) | 6×10^{17} | ---- | Te | ---- | 3600 | 0.18 | | 0.18 |
| - " - | 1.15×10^{18} | ---- | S | ---- | 2600 | 0.31 | | 0.25 |
| - " - | 1.2×10^{18} | ---- | Te | ---- | 3100 | 0.22 | | 0.22 |

*Intentionally compensated with Ge (see text).

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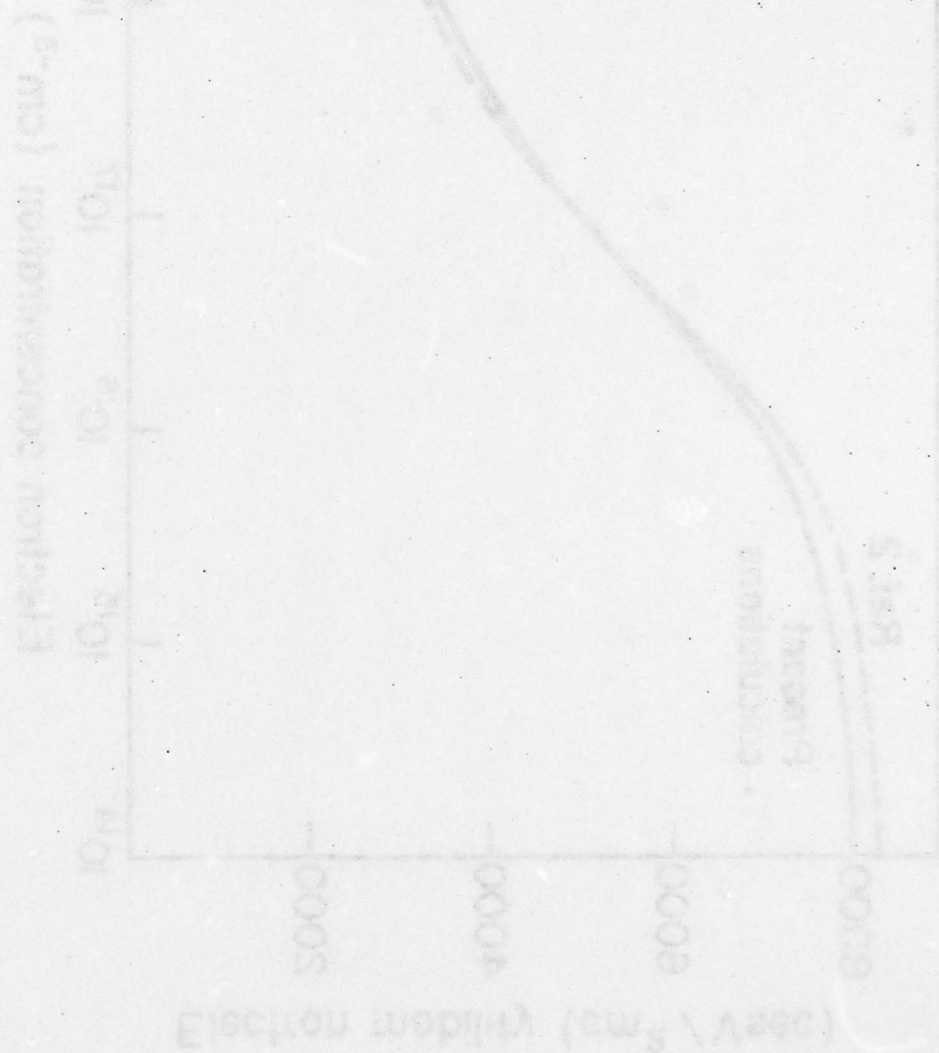
(38) The accuracy of the variational principle method increases with decreasing $z_l = \frac{\hbar\omega_0}{kT}$. For GaAs at room temperature $z_l \approx 1.4$. A comparison of results in ref (4) and recent calculations in ref (39) shows that the accuracy of variational calculations in the form presented here can be expected to be better than 5%.

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FIGURE CAPTIONS

- Figure 1. Comparison of electron mobilities calculated by a variational method (present calculations) and by an iterative procedure (ref. 2) for n-type GaAs at room temperature; screening of polar scattering is not included (see text).
- Figure 2. Calculated component and total electron mobility as a function of electron concentration in n-type GaAs at room temperature.
- Figure 3. Comparison of electron mobilities in n-type GaAs calculated by a variational method and by Matthiessen's rule employing the component mobilities.
- Figure 4. Theoretical (solid lines) and experimental values of mobility as a function of electron concentration in n-type GaAs for various compensation ratios; the mobility range for commercially available GaAs is also indicated.
- Figure 5. Theoretical and experimental values of absorption coefficient as a function of electron concentration in GaAs at room temperature.
- Figure 6. Theoretical (solid line) and experimental values of absorption coefficient reduced to zero compensation (see text) as a function of electron concentration in GaAs at room temperature; wavelength of radiation $\lambda = 10 \mu\text{m}$.
- Figure 7. Absorption coefficient as a function of wavelength.

Solid and dotted lines correspond to theoretical values, neglecting compensation, and dotted lines correspond to theoretical values obtained by taking into account compensation as determined from electron mobility; ●, ■ and ▲ are experimental values obtained with samples 6, 3 and 2, respectively, of GaAs as in Table III.



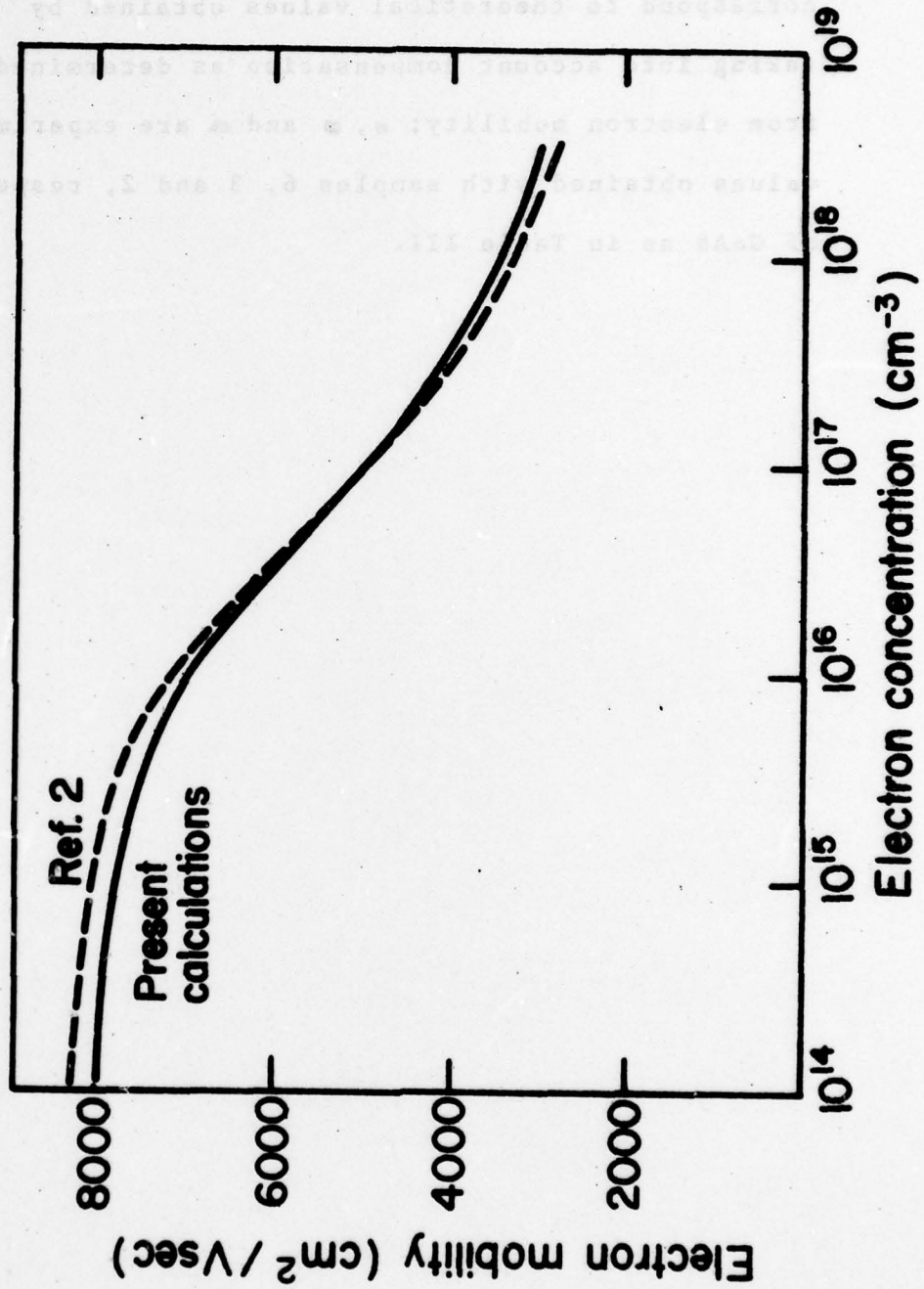


Figure 1

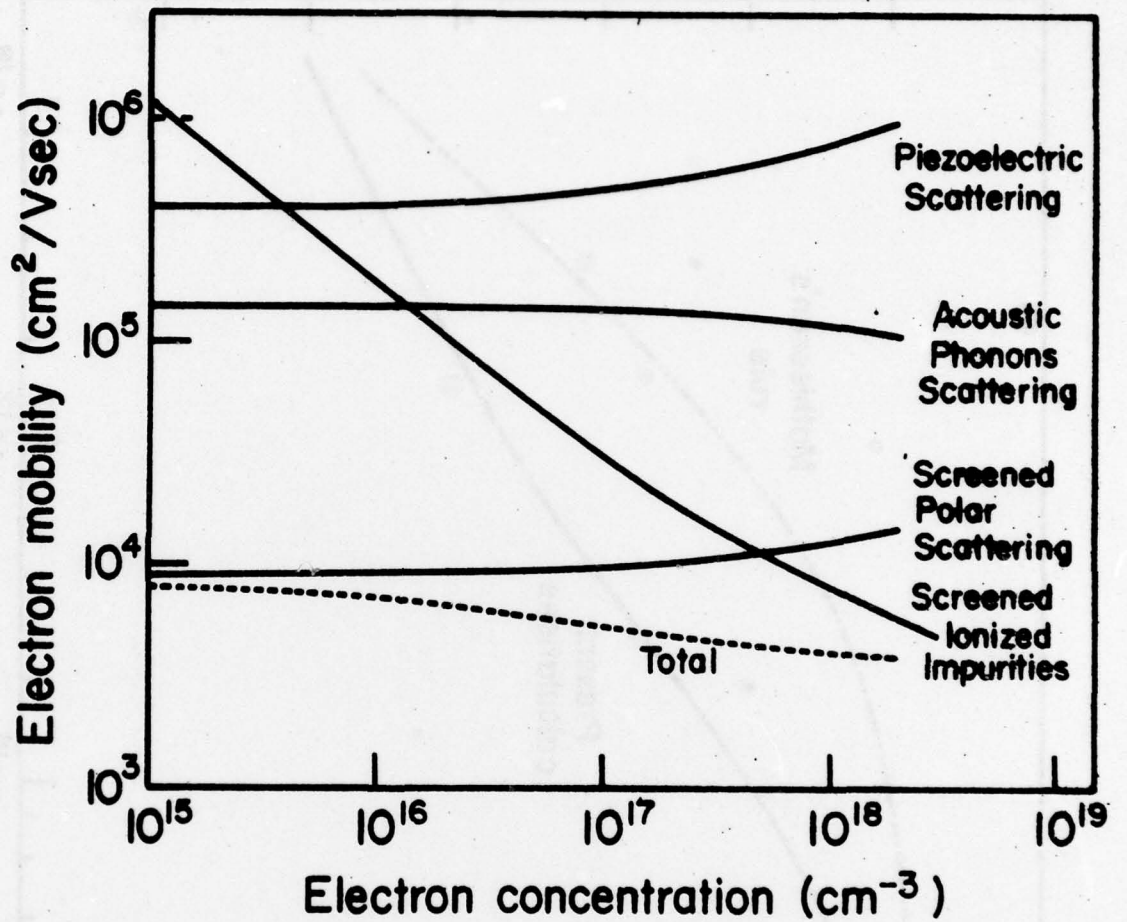


Figure 2

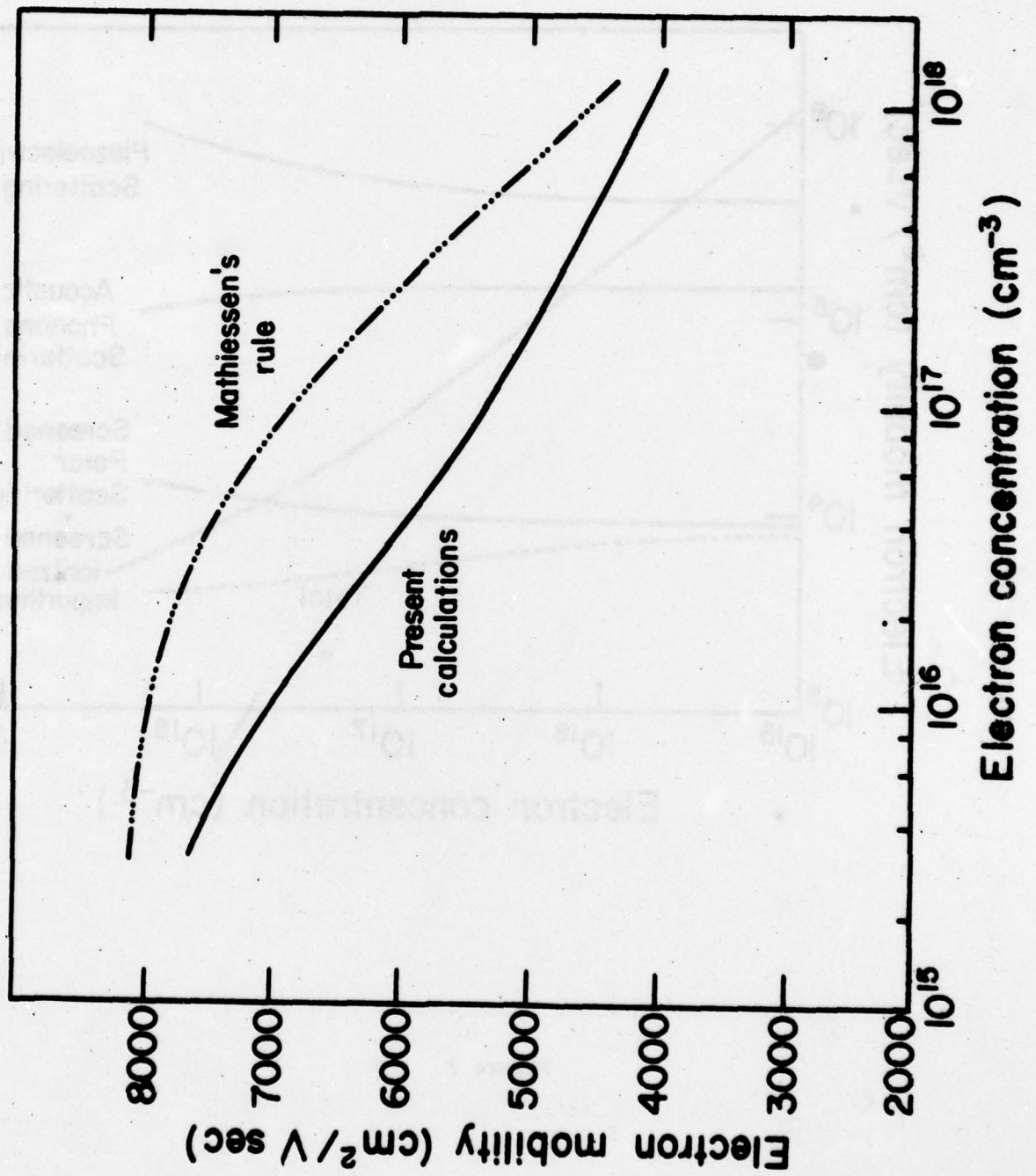


Figure 3

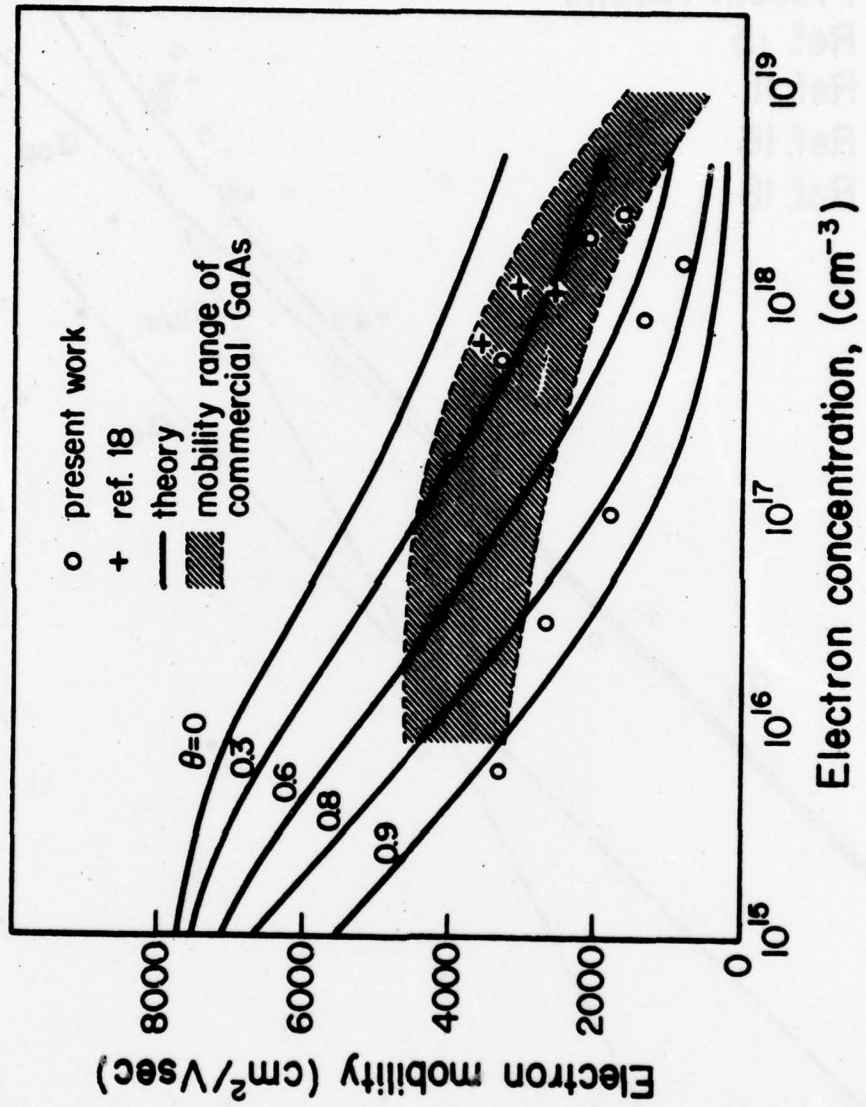


Figure 4

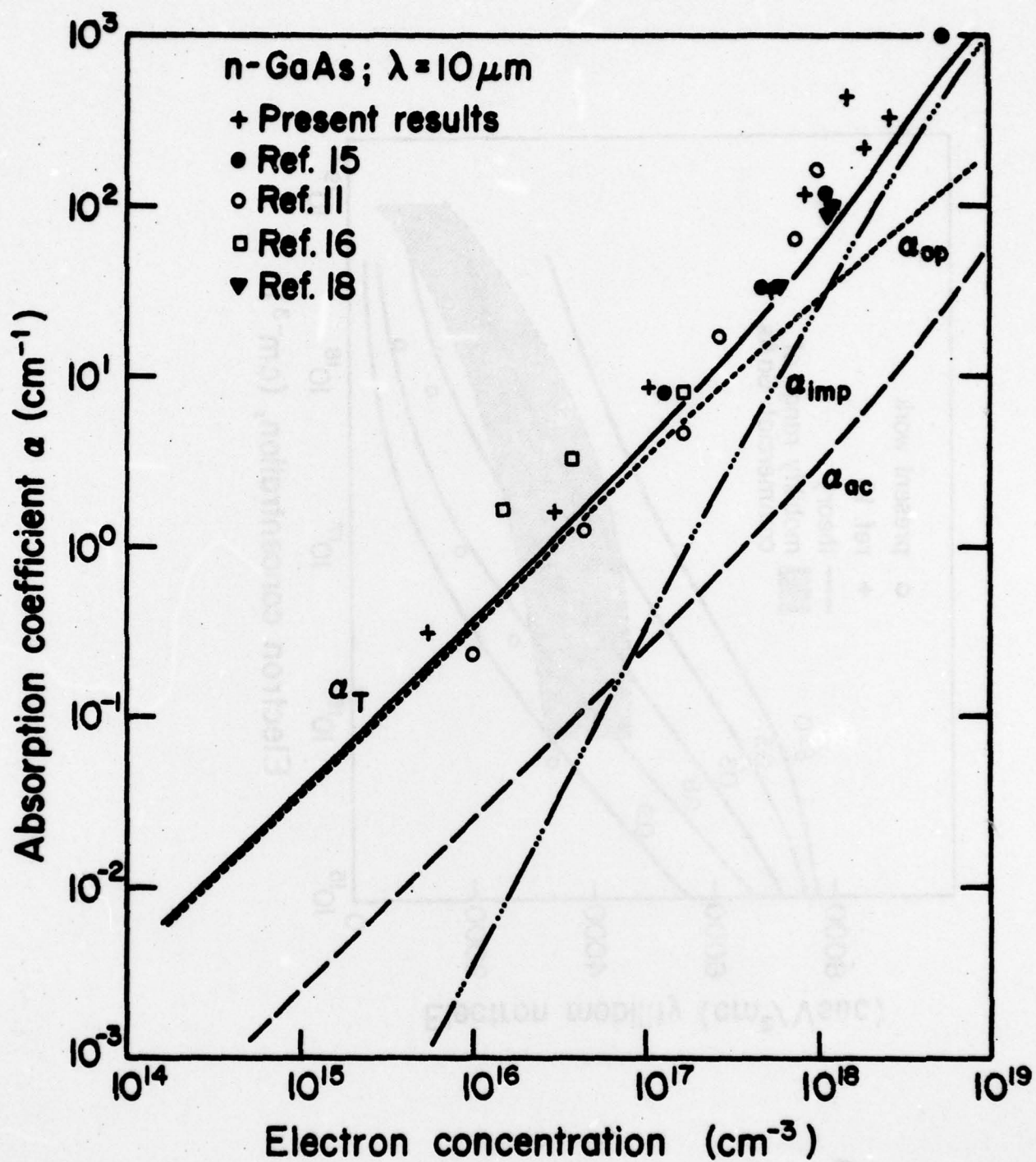


Figure 5

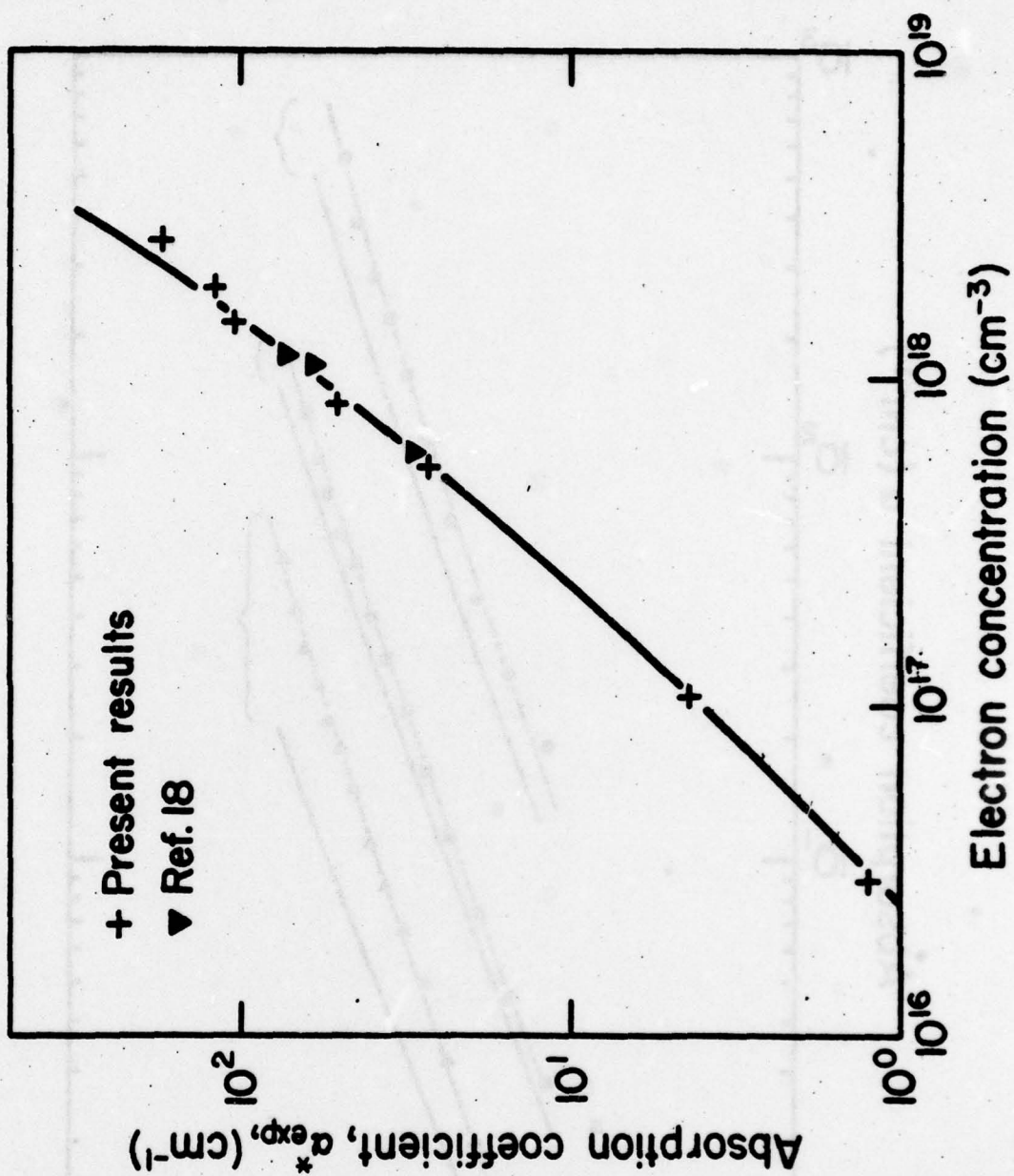


Figure 6

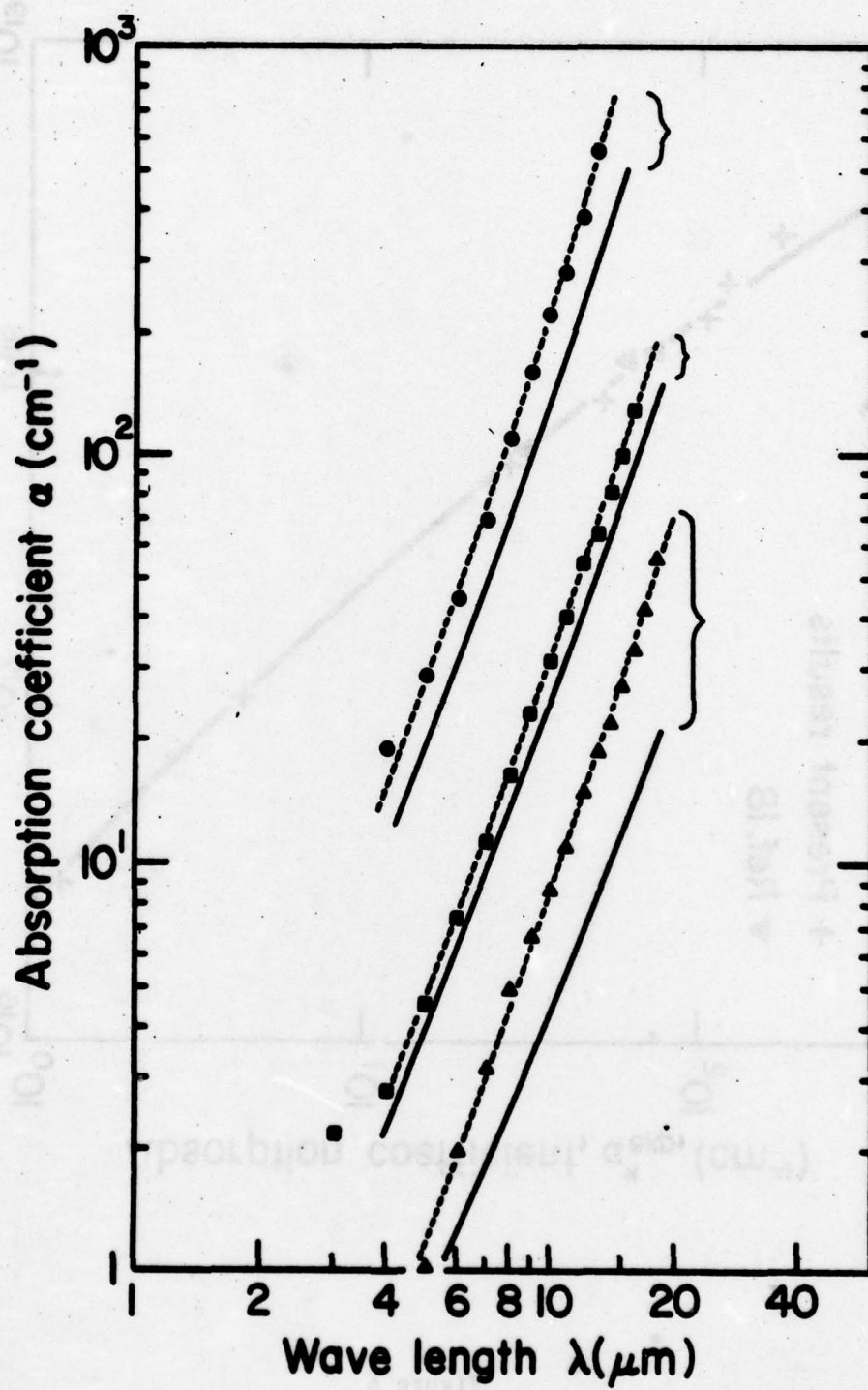


Figure 7



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